



**Universitat**  
de les Illes Balears



***TRAM***  
***(Triangle-based Regional Atmospheric Model)***

***A New Nonhydrostatic Fully Compressible  
Numerical Model***

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MINISTERIO  
DE ECONOMÍA, INDUSTRIA  
Y COMPETITIVIDAD



**COASTEPS**  
**CGL2017-82868-R**



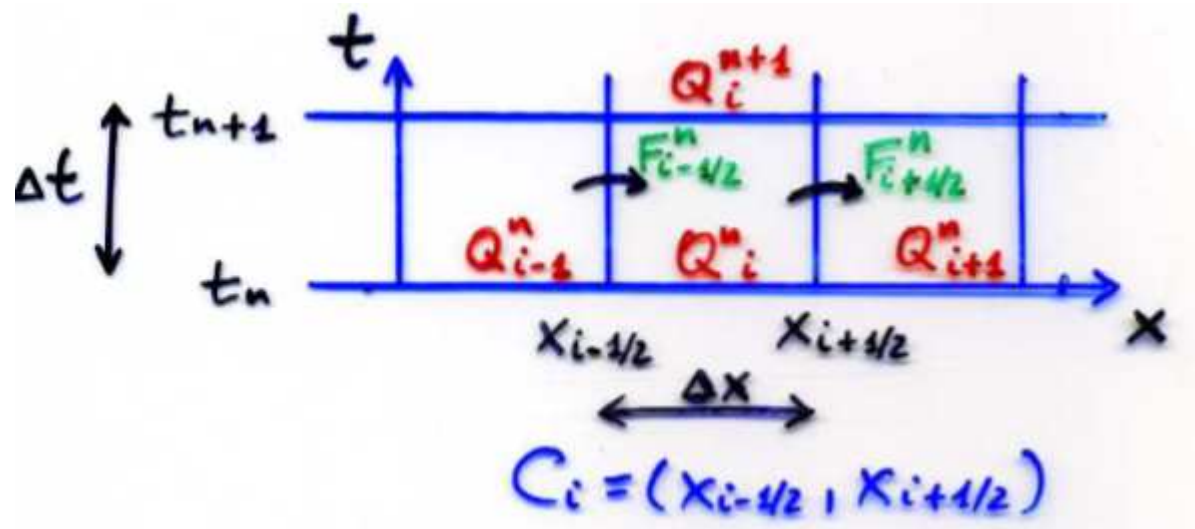
**EUROPEAN UNION**  
EUROPEAN REGIONAL  
DEVELOPMENT FUND  
"A way to make Europe"

- > WHY NOT our own model ? (e.g. GLOBO-BOLAM-MOLOCH)
- > Mostly for RESEARCH and ACADEMIC purposes, but potentially for "FORECASTING" as well
- > Aimed at MESOSCALE applications and IDEALIZED experiments (high resolution and regional contexts), although naturally suited to SYNOPTIC scale
- > The new numerical model must necessarily involve ORIGINAL aspects and pass some benchmark TESTS

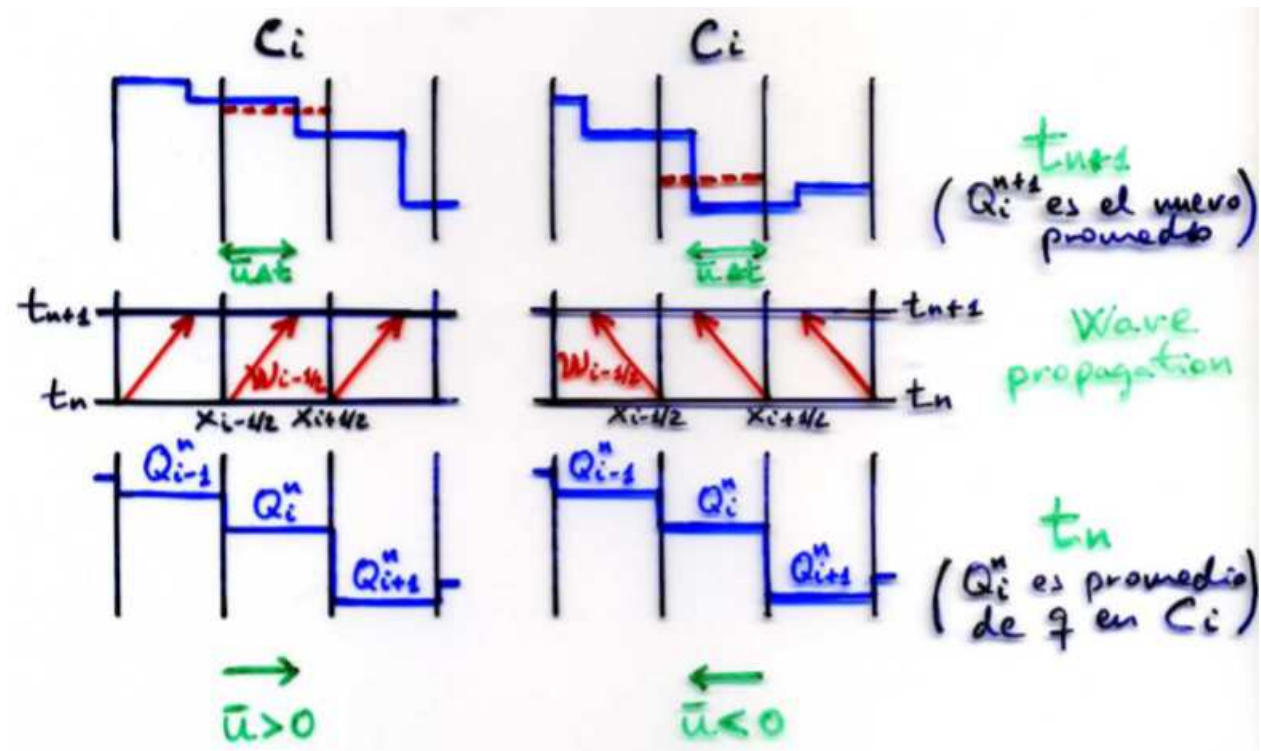
>  $\partial_t q = -\bar{u} \partial_x q$  expressed in flux form is  $\partial_t q = -\partial_x(\bar{u} q)$

> The new cell average  $Q_i^{n+1}$  would be approximated as

$$Q_i^{n+1} = Q_i^n - \frac{\Delta t}{\Delta x} (F_{i+1/2}^n - F_{i-1/2}^n)$$



## > REA (Reconstruct-Evolve-Average) point of view



## > Classical choices for the slopes

$$\sigma_i^n = 0$$

Up Wind

$$\sigma_i^n = \frac{Q_{i+1}^n - Q_i^n}{\Delta x}$$

LW

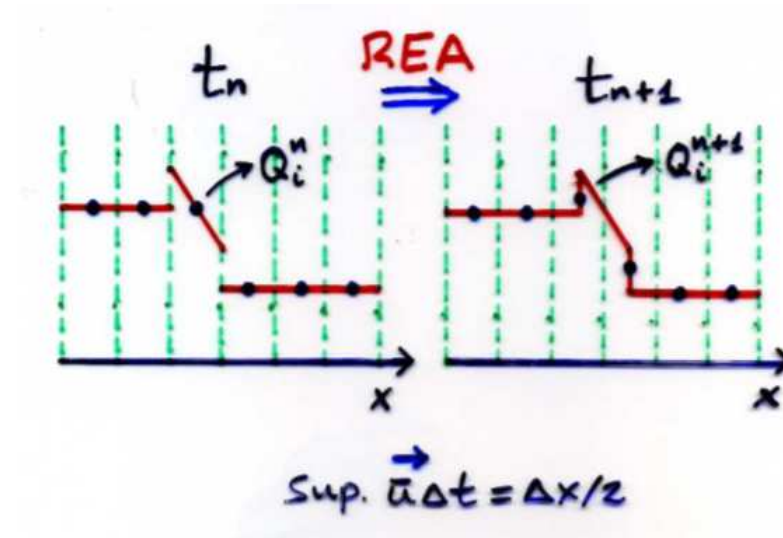
$$\sigma_i^n = \frac{Q_i^n - Q_{i-1}^n}{\Delta x}$$

BW

$$\sigma_i^n = \frac{Q_{i+1}^n - Q_{i-1}^n}{2\Delta x}$$

Fromm





## > Slope-Limiter methods

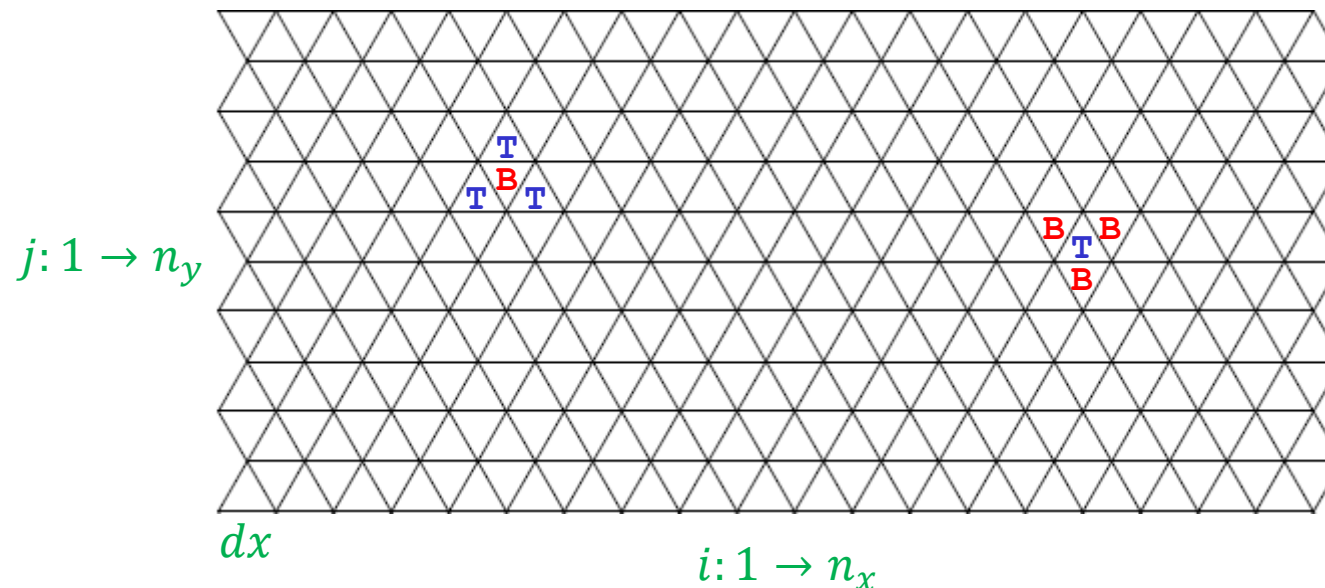
$$\sigma_i^n = \minmod\left(\frac{LW}{BW}\right) \quad \sigma_i^n = \minmod\left(\frac{2 LW}{2 BW}, \text{Fromm}\right) \quad \sigma_i^n = \maxmod\left(\begin{matrix} \minmod\left(\frac{LW}{2 BW}\right) \\ \minmod\left(\frac{2 LW}{BW}\right) \end{matrix}\right)$$

Minmod
MC
Superbee

> REA also for  $\partial_t q = -u \partial_x q$  (e.g.  $q = u$ ) using  $U_{i+1/2}^n = \frac{U_i^n + U_{i+1}^n}{2}$

> Linear profile for wind within cell:  $x' = U_{i+1/2}^n + Ax$

## > Triangular-based mesh



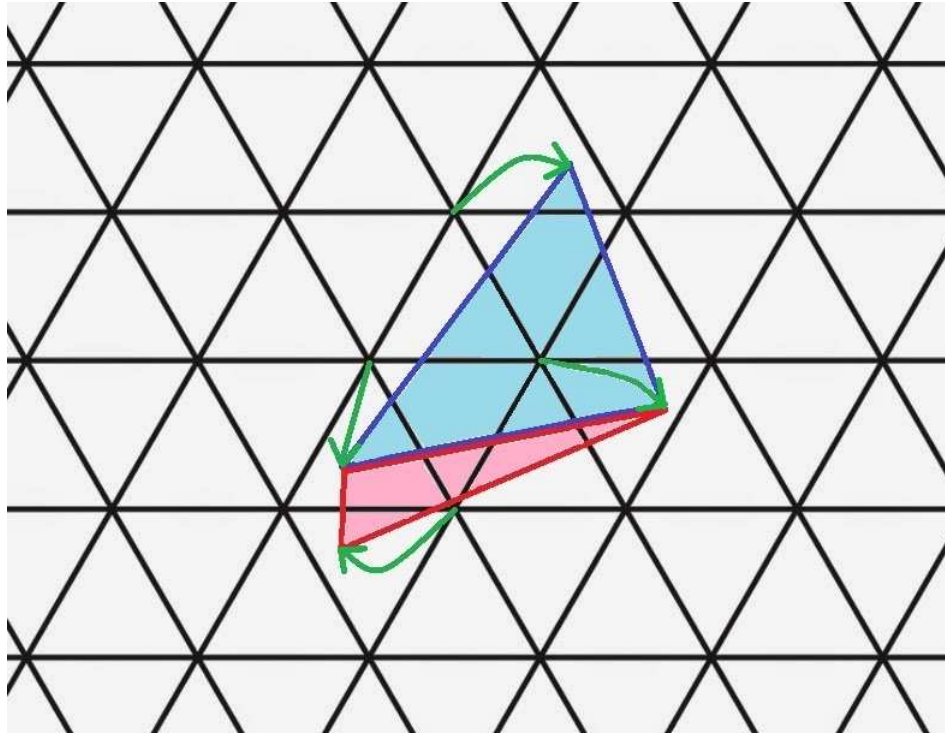
> Actual **resolution** (square-based domain) is  $\approx \frac{2}{3}dx$

> All **variables** defined at triangle barycenters:  $T_{ij}$   $B_{ij}$

> 1<sup>st</sup> **derivatives** (slopes) at  $T/B$  from neighbor  $B/T$

> 2<sup>nd</sup> **derivatives** (e.g. diffusion) using all four  $T/B$

- > True 2D REA instead of dimensional splitting

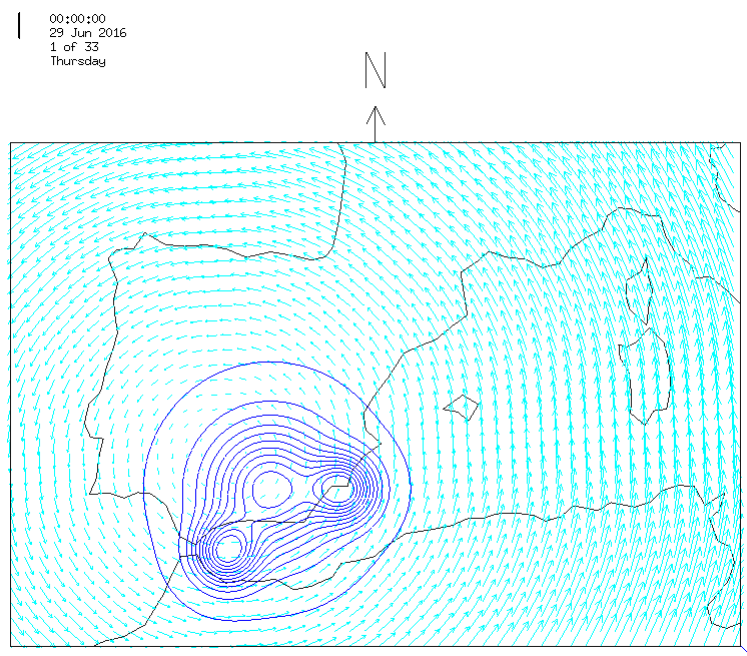


- > MC Slope Limiter, using local and neighbor slopes
- > 6-cell average wind at corners  $\bar{U}_{ij}^n$   $\bar{V}_{ij}^n$
- > Linear profile for wind within cell: 
$$\begin{cases} x' = \bar{U}_{ij}^n + Ax + By \\ y' = \bar{V}_{ij}^n + Cx + Dy \end{cases}$$

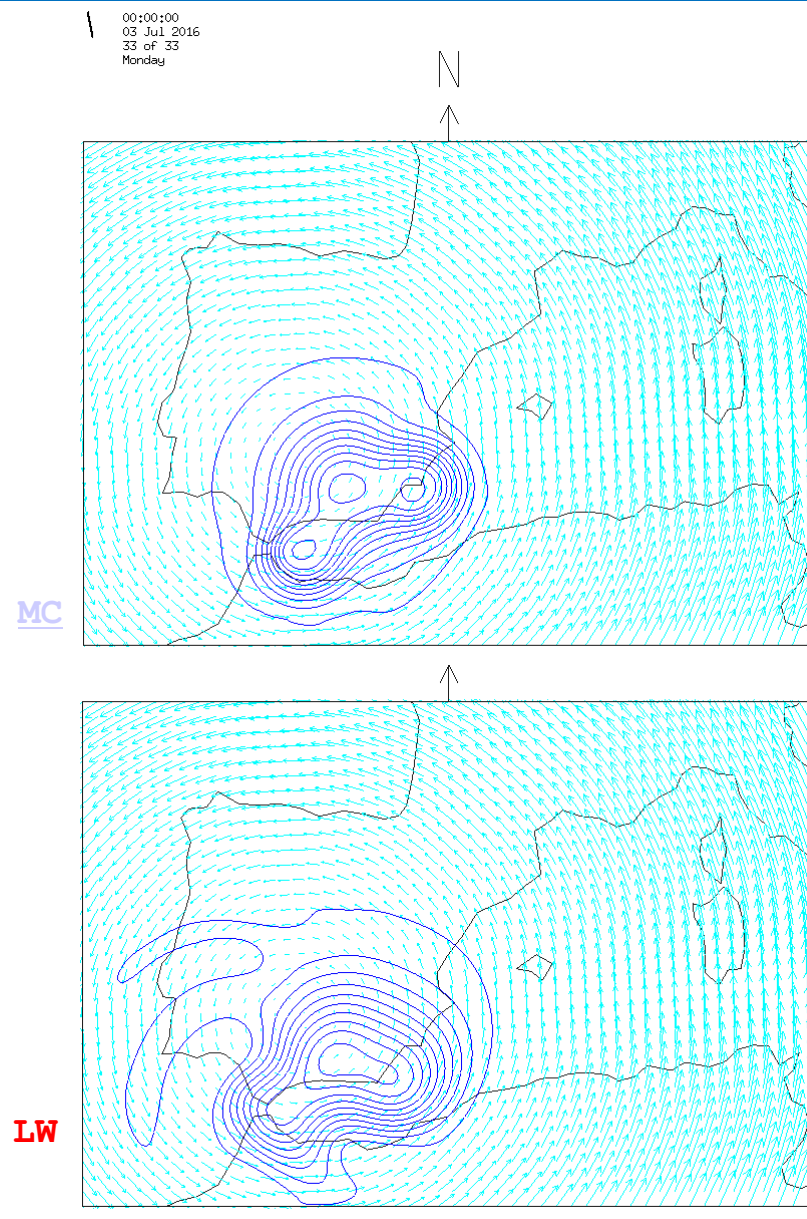
## > Rotating Gaussians

(dx=20km, dt=60s, 4revs/4days)

(NO wind profile)



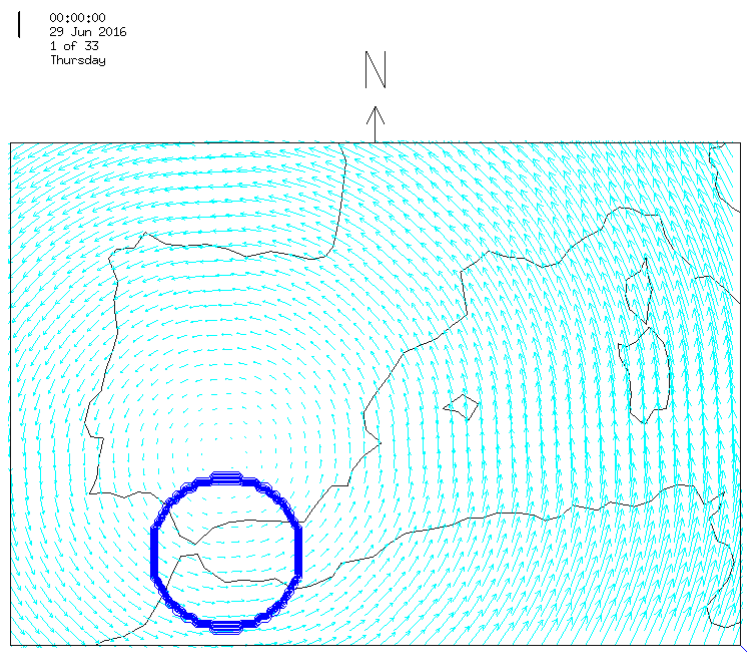
Initial



## > Rotating Cylinder

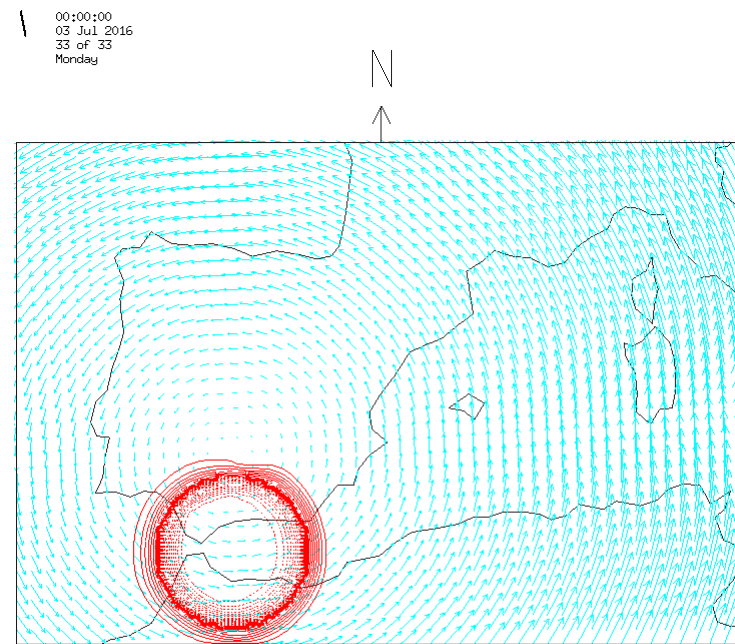
(dx=20km, dt=60s, 4revs/4days)

(+ wind profile)

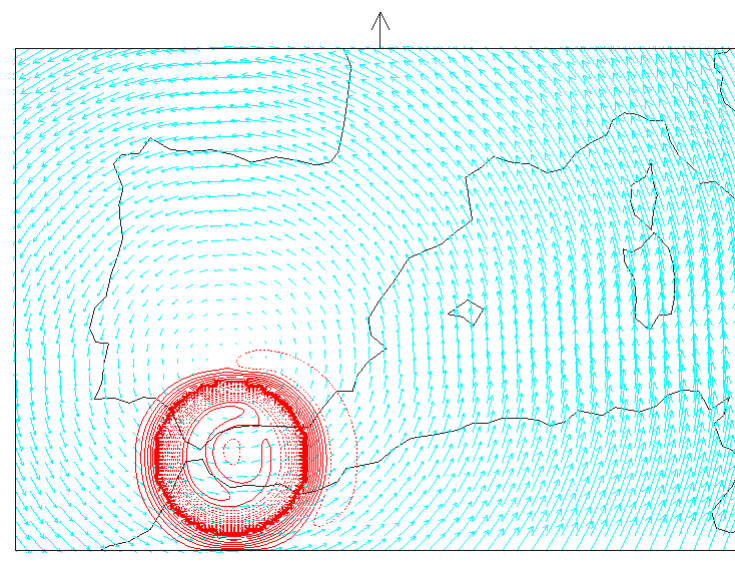


Initial

MC



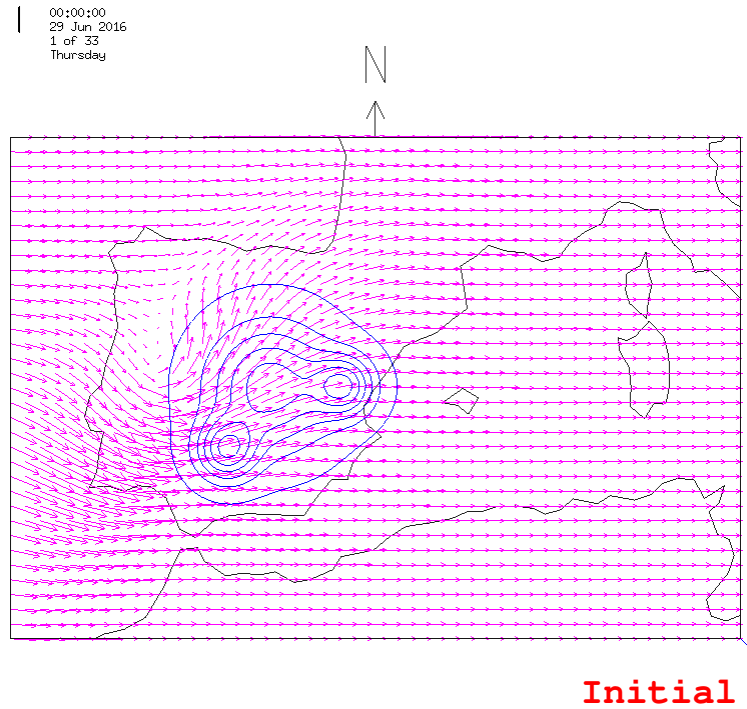
Fromm



## > Vortex in zonal flow

(dx=20km, dt=180s, Periodic BCs, 4days)

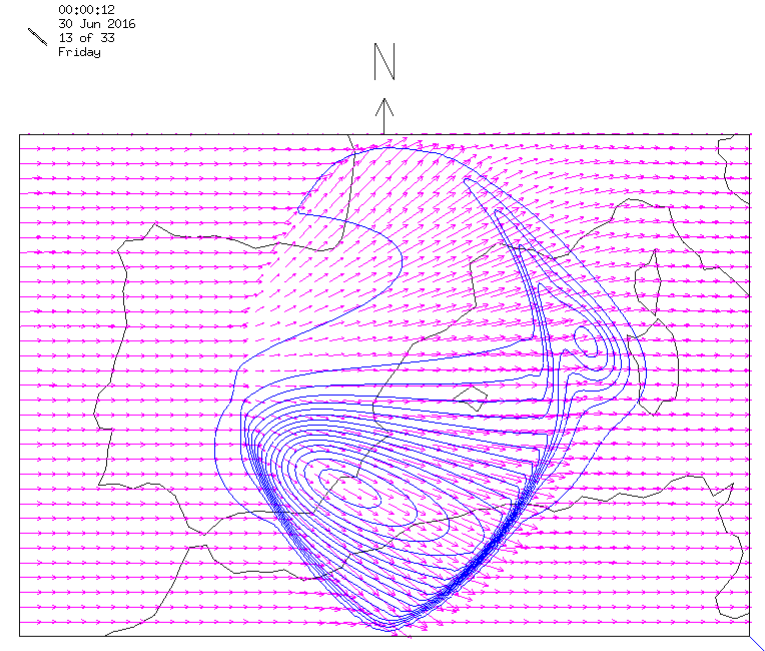
(+ episodic source  $S$ )



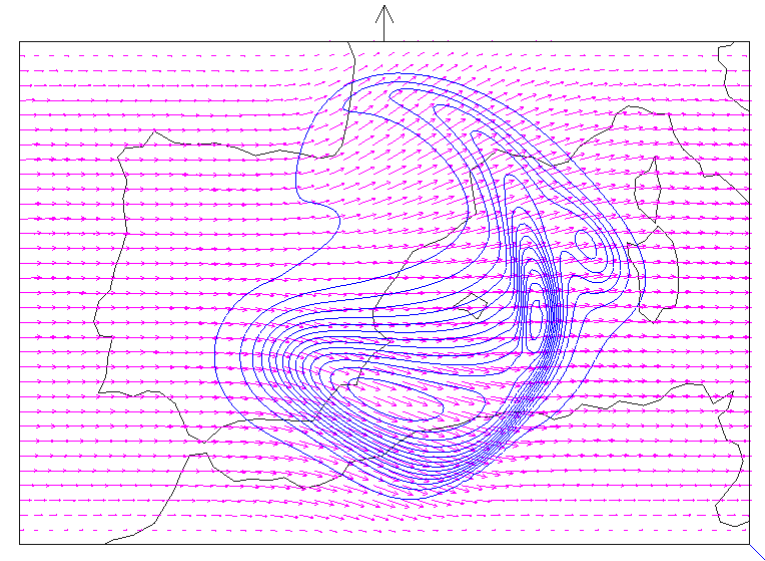
$$\frac{d\vec{V}}{dt} = \vec{D} \begin{cases} \partial_t u = -u\partial_x u - v\partial_y u + k\nabla^2 u \\ \partial_t v = -u\partial_x v - v\partial_y v + k\nabla^2 v \end{cases}$$

$$\partial_t \phi = -u\partial_x \phi - v\partial_y \phi + S$$

NO  $\vec{D}$



+  $\vec{D}$



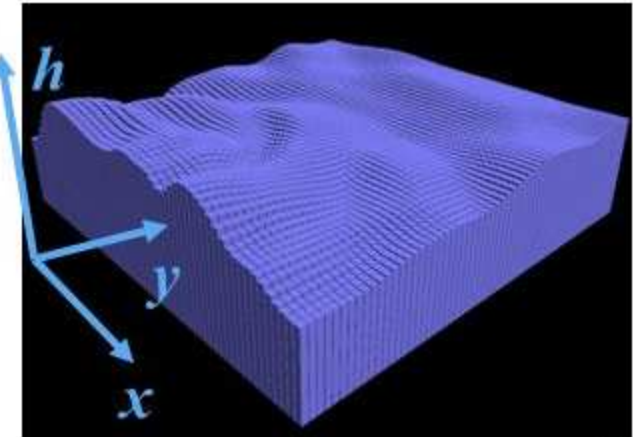


## > Governing equations

$$\frac{\partial h}{\partial t} = -u \frac{\partial h}{\partial x} - v \frac{\partial h}{\partial y} - h \left[ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right]$$

$$\frac{\partial u}{\partial t} = -u \frac{\partial u}{\partial x} - v \frac{\partial u}{\partial y} - g \frac{\partial h}{\partial x} + fv - bu + \mu \nabla^2 u$$

$$\frac{\partial v}{\partial t} = -u \frac{\partial v}{\partial x} - v \frac{\partial v}{\partial y} - g \frac{\partial h}{\partial y} - fu - bv + \mu \nabla^2 v$$



## > Numerical implementation

- \* **Forward-Backward** integration of “forcings” in **RK** cycle

$$\text{RK2} \quad \begin{cases} \phi^* = \phi^n + \frac{\Delta t}{2} F(\phi^n) \\ \phi^{n+1} = \phi^n + \Delta t F(\phi^*) \end{cases} \quad \text{SSPRK2} \quad \begin{cases} \phi^* = \phi^n + \Delta t F(\phi^n) \\ \phi^{**} = \phi^* + \Delta t F(\phi^*) \\ \phi^{n+1} = \frac{1}{2}(\phi^n + \phi^{**}) \end{cases} \quad \text{CFL} \xrightarrow{\sqrt{gH}} \Delta t$$

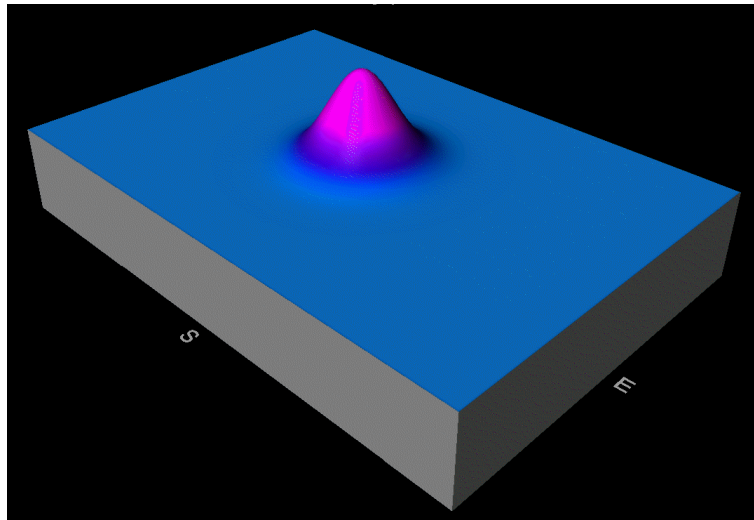
- \* **REA** integration of **advective terms** at end of timestep

- \* Rigid **Wall BCs** at the 4 boundaries

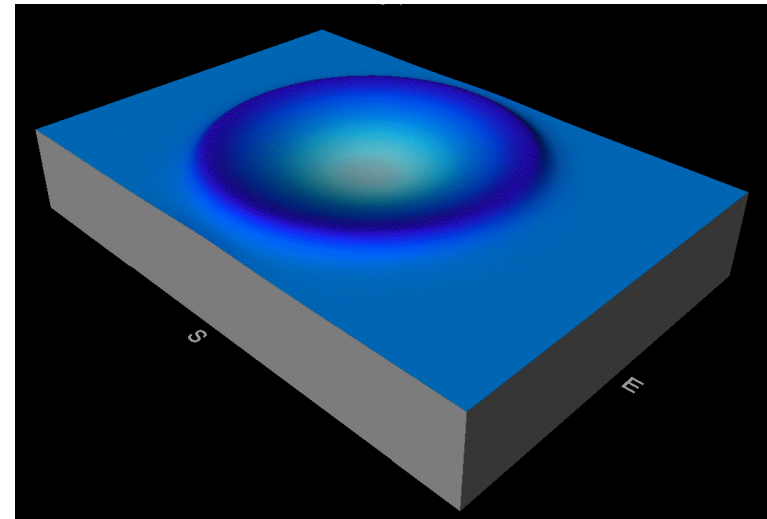
# > Gaussian Bump in H=10m

(dx=20km, dt=180s, 2000x1600km, 10days)

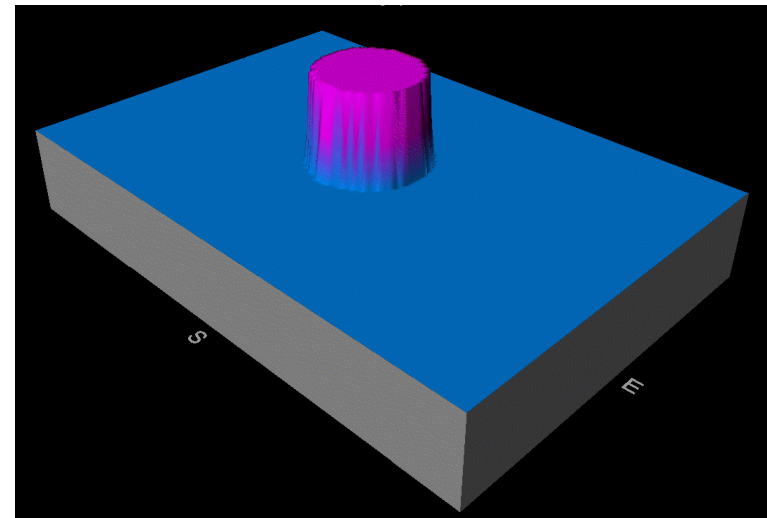
(NO Coriolis/Drag/Diffusion)



Initial



RK2



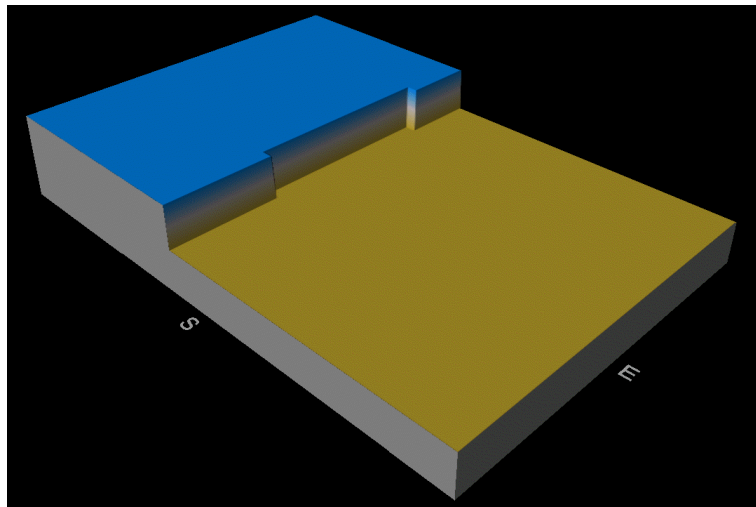
SSPRK2



# > Partial Dam Break 10-5 m

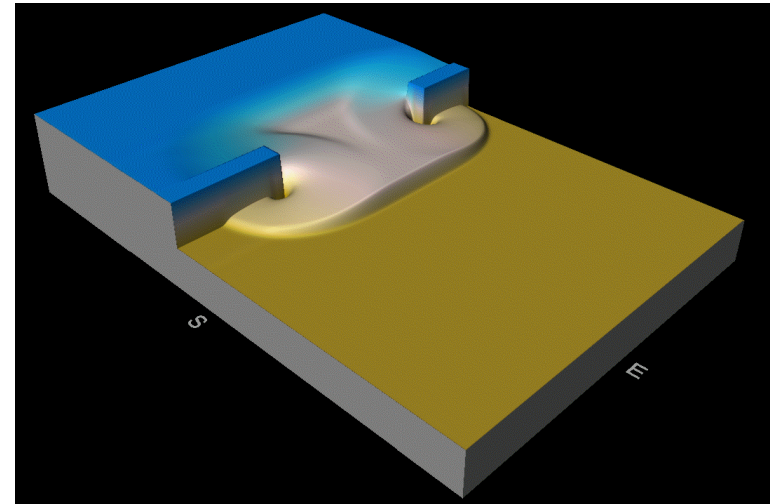
(dx=5km, dt=180s, 2000x1600km, 10days)

(NO Coriolis/Drag/Diffusion)

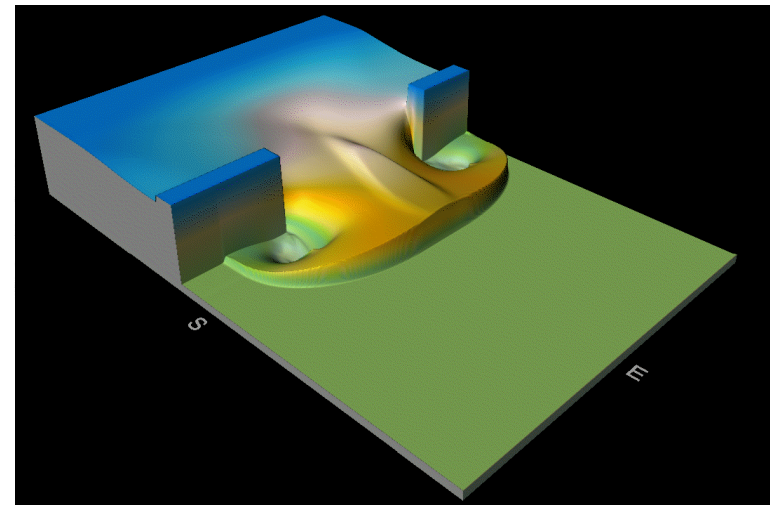


Initial

SSPRK2



10-1 m



# Non-Hydrostatic Fully-Compressible Equations

> Combine the fundamental principles

$$\frac{dT}{dt} = \frac{1}{c_p \rho} \frac{dP}{dt} \quad P = \rho R T \quad \text{Adiabatic atmosphere}$$

$$\frac{d\rho}{dt} = -\rho \left[ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right] \quad \text{No moisture}$$

$$\frac{du}{dt} = -\frac{1}{\rho} \frac{\partial P}{\partial x} + f v - \hat{f} w \quad \text{Inviscid flow}$$

$$\frac{dv}{dt} = -\frac{1}{\rho} \frac{\partial P}{\partial y} - f u$$

$$\frac{dw}{dt} = -\frac{1}{\rho} \frac{\partial P}{\partial z} - g + \hat{f} u$$

> in terms of the following variables

$$\text{Exner pressure: } \pi = \left( \frac{P}{P_0} \right)^{R/c_p} \quad \text{Potential temperature: } \theta = \frac{T}{\pi}$$

# Non-Hydrostatic Fully-Compressible Equations

## > Alternative version of Euler equations

$$\frac{\partial \pi}{\partial t} = -u \frac{\partial \pi}{\partial x} - v \frac{\partial \pi}{\partial y} - w \frac{\partial \pi}{\partial z} - \frac{R}{c_v} \pi \left[ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right]$$

$$\frac{\partial \theta}{\partial t} = -u \frac{\partial \theta}{\partial x} - v \frac{\partial \theta}{\partial y} - w \frac{\partial \theta}{\partial z}$$

$$\frac{\partial u}{\partial t} = -u \frac{\partial u}{\partial x} - v \frac{\partial u}{\partial y} - w \frac{\partial u}{\partial z} - c_p \theta \frac{\partial \pi}{\partial x} + f v - \hat{f} w$$

$$\frac{\partial v}{\partial t} = -u \frac{\partial v}{\partial x} - v \frac{\partial v}{\partial y} - w \frac{\partial v}{\partial z} - c_p \theta \frac{\partial \pi}{\partial y} - f u$$

$$\frac{\partial w}{\partial t} = -u \frac{\partial w}{\partial x} - v \frac{\partial w}{\partial y} - w \frac{\partial w}{\partial z} - c_p \theta \frac{\partial \pi}{\partial z} - g + \hat{f} u$$

## > Apply the following decomposition

$$\left. \begin{aligned} \pi(x, y, z, t) &= \bar{\pi}(z) + \pi'(x, y, z, t) \\ \theta(x, y, z, t) &= \bar{\theta}(z) + \theta'(x, y, z, t) \end{aligned} \right\} c_p \bar{\theta} \frac{\partial \bar{\pi}}{\partial z} = -g \quad \text{Hydrostatic balance}$$

# Non-Hydrostatic Fully-Compressible Equations

> **FINAL** version of Euler (Navier-Stokes) equations

$$\frac{\partial \pi'}{\partial t} = -u \frac{\partial \pi'}{\partial x} - v \frac{\partial \pi'}{\partial y} - w \frac{\partial \pi'}{\partial z} - w \frac{\partial \bar{\pi}}{\partial z} - \frac{R}{c_v} (\bar{\pi} + \pi') \left[ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right]$$

$$\frac{\partial \theta'}{\partial t} = -u \frac{\partial \theta'}{\partial x} - v \frac{\partial \theta'}{\partial y} - w \frac{\partial \theta'}{\partial z} - w \frac{\partial \bar{\theta}}{\partial z} + \mu \left[ \nabla^2 \theta' + \frac{\partial^2 (\bar{\theta} + \theta')}{\partial z^2} \right]$$

$$\frac{\partial u}{\partial t} = -u \frac{\partial u}{\partial x} - v \frac{\partial u}{\partial y} - w \frac{\partial u}{\partial z} - c_p (\bar{\theta} + \theta') \frac{\partial \pi'}{\partial x} + f v - \hat{f} w + \mu \left[ \nabla^2 u + \frac{\partial^2 u}{\partial z^2} \right]$$

$$\frac{\partial v}{\partial t} = -u \frac{\partial v}{\partial x} - v \frac{\partial v}{\partial y} - w \frac{\partial v}{\partial z} - c_p (\bar{\theta} + \theta') \frac{\partial \pi'}{\partial y} - f u + \mu \left[ \nabla^2 v + \frac{\partial^2 v}{\partial z^2} \right]$$

$$\frac{\partial w}{\partial t} = -u \frac{\partial w}{\partial x} - v \frac{\partial w}{\partial y} - w \frac{\partial w}{\partial z} - c_p (\bar{\theta} + \theta') \frac{\partial \pi'}{\partial z} + g \frac{\theta'}{\bar{\theta}} + \hat{f} u + \mu \left[ \nabla^2 w + \frac{\partial^2 w}{\partial z^2} \right]$$

> Numerical implementation 3D [CFL  $\xrightarrow{c_s > 300 \text{ m/s}}$   $\Delta t \approx 2 \Delta x (\Delta z)$ ]

- \* Forward-Backward integration of "forcings" in RK2 cycle
- \* REA (V and H) integration of advection every 6-10 Nsteps
- \* Rigid Wall BCs at W/E S/N B/T boundaries

# Non-Hydrostatic Fully-Compressible Equations

> **FINAL** version of Euler (Navier-Stokes) equations

$$\frac{\partial \pi'}{\partial t} = -u \frac{\partial \pi'}{\partial x} - \cancel{v \frac{\partial \pi'}{\partial y}} - w \frac{\partial \pi'}{\partial z} - w \frac{\partial \bar{\pi}}{\partial z} - \frac{R}{c_v} (\bar{\pi} + \pi') \left[ \frac{\partial u}{\partial x} + \cancel{\frac{\partial v}{\partial y}} + \frac{\partial w}{\partial z} \right]$$

$$\frac{\partial \theta'}{\partial t} = -u \frac{\partial \theta'}{\partial x} - \cancel{v \frac{\partial \theta'}{\partial y}} - w \frac{\partial \theta'}{\partial z} - w \frac{\partial \bar{\theta}}{\partial z} + \mu \left[ \nabla_x^2 \theta' + \frac{\partial^2 (\bar{\theta} + \theta')}{\partial z^2} \right]$$

$$\frac{\partial u}{\partial t} = -u \frac{\partial u}{\partial x} - \cancel{v \frac{\partial u}{\partial y}} - w \frac{\partial u}{\partial z} - c_p (\bar{\theta} + \theta') \frac{\partial \pi'}{\partial x} + \cancel{fv} - \cancel{\hat{f}w} + \mu \left[ \nabla_x^2 u + \frac{\partial^2 u}{\partial z^2} \right]$$

**2D (NO rotation)**

$$\frac{\partial w}{\partial t} = -u \frac{\partial w}{\partial x} - \cancel{v \frac{\partial w}{\partial y}} - w \frac{\partial w}{\partial z} - c_p (\bar{\theta} + \theta') \frac{\partial \pi'}{\partial z} + g \frac{\theta'}{\bar{\theta}} + \cancel{\hat{f}u} + \mu \left[ \nabla_x^2 w + \frac{\partial^2 w}{\partial z^2} \right]$$

> Numerical implementation 2D [CFL  $\xrightarrow{c_s > 300 \text{ m/s}}$   $\Delta t \approx 3 \Delta x (\Delta z)$ ]

- \* Forward-Backward integration of "forcings" in RK2 cycle
- \* REA (V and H) integration of advection every 6-10 Nsteps
- \* Rigid Wall BCs at W/E B/T boundaries

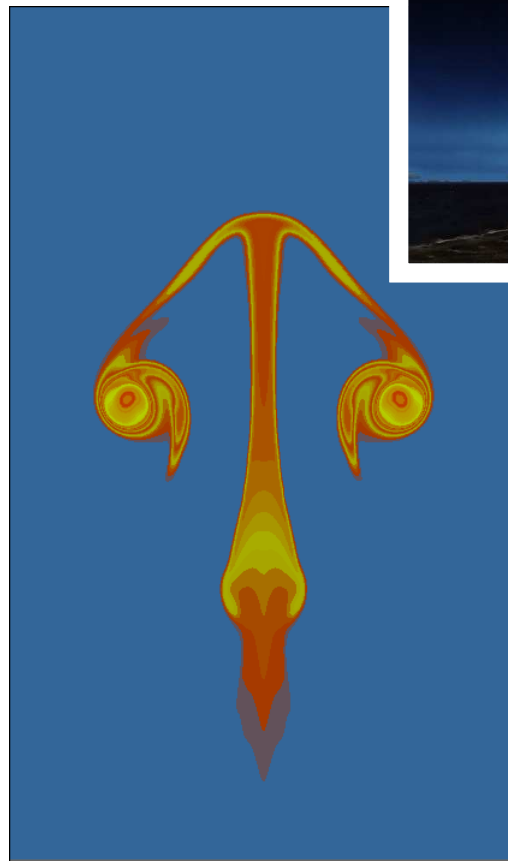
# > Rising Thermal Bubble (calm and neutrally-stable environment)

(dx=dz=100m, dt=0.2s, Nstep=10, 50min)

(NO Coriolis/Diffusion)



Initial



3D

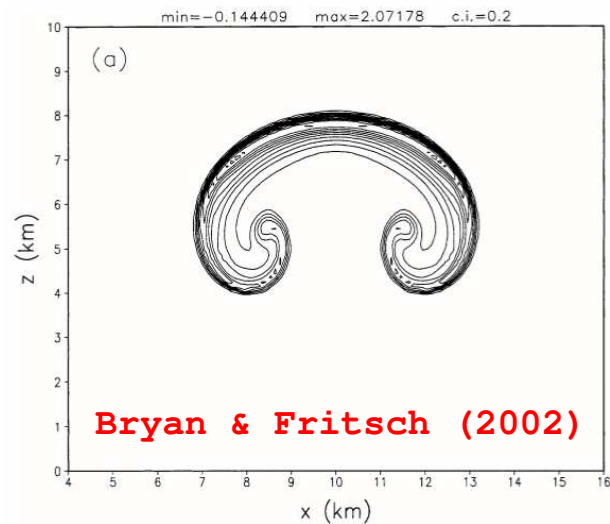
\* Check of MASS & Total ENERGY

$$\Delta M = -0.002 \%$$

$$\Delta E = -0.0005 \%$$

## > Rising Thermal Bubble (2D)

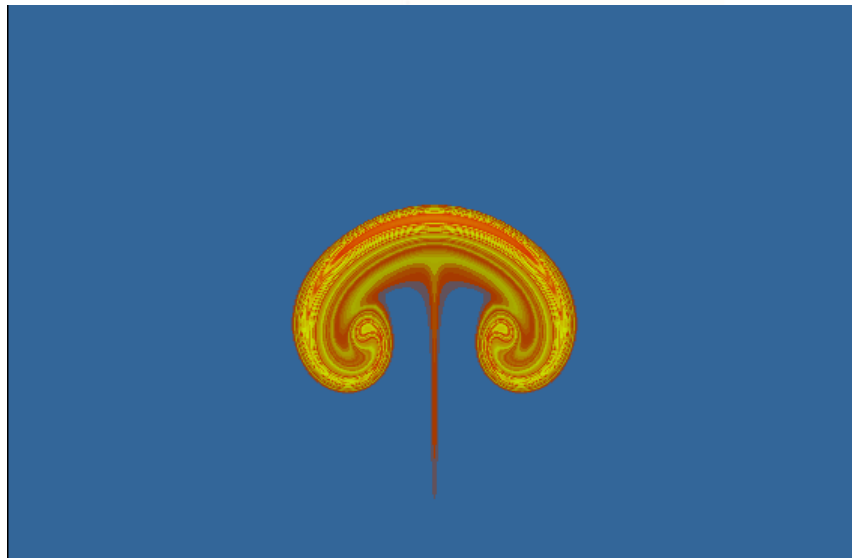
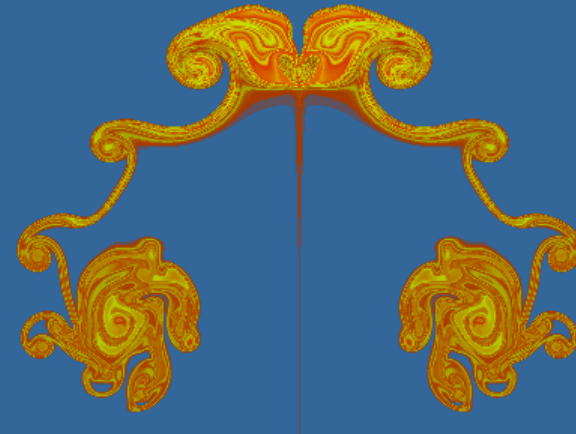
(dx=dz=50m, dt=0.125s, Nstep=10, 55min)



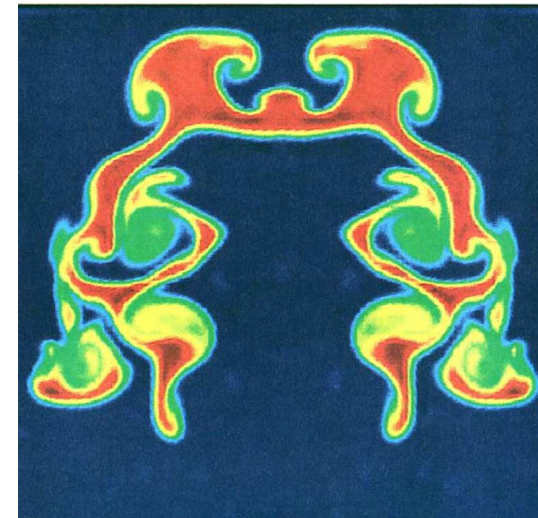
Double resolution

t=33min

$\Delta M = +0.0003 \%$   $\Delta E = +0.0002 \%$



t=17min



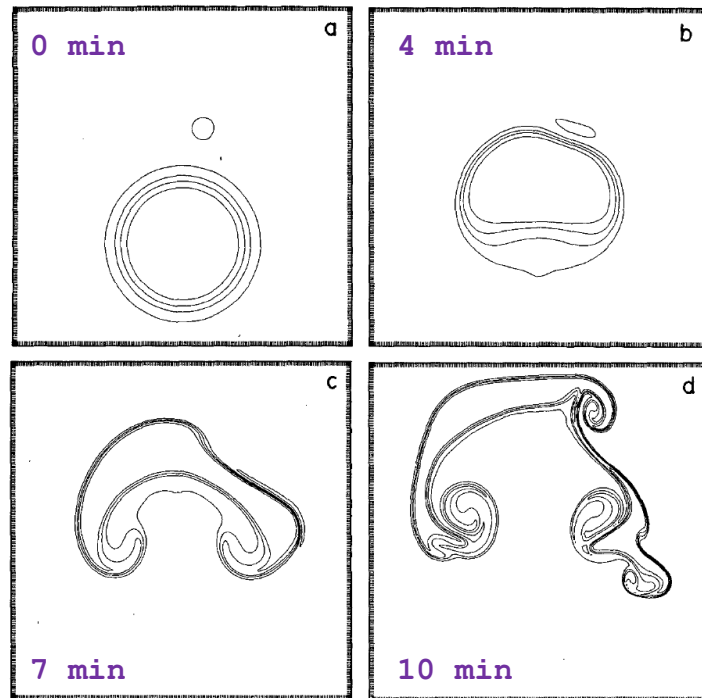
Robert (1993)



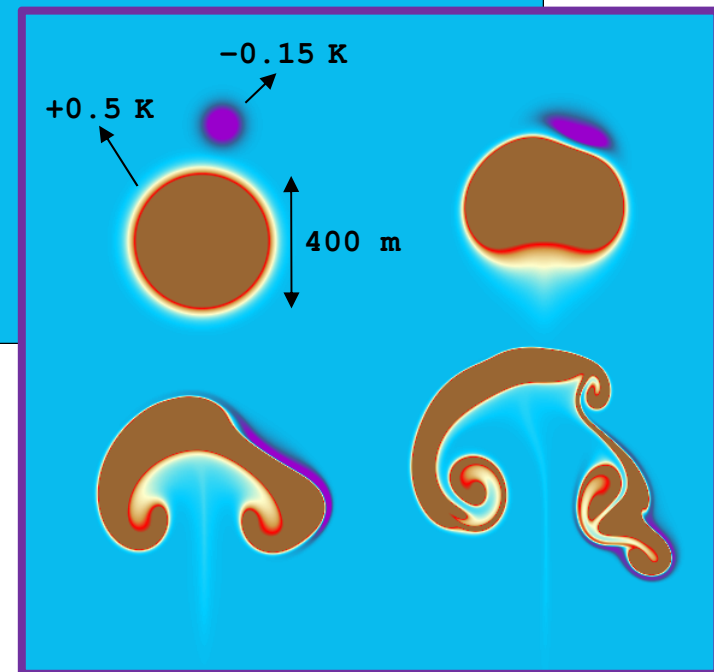
## > Large Warm & Small Cold Bubbles

( $dx=dz=2.5m$ ,  $dt=0.00625s$ ,  $Nstep=10$ , 40min)

Robert (1993)



Initial



$$\Delta M = -0.00007 \%$$

$$\Delta E = -0.0001 \%$$

Animation

## > Density Current

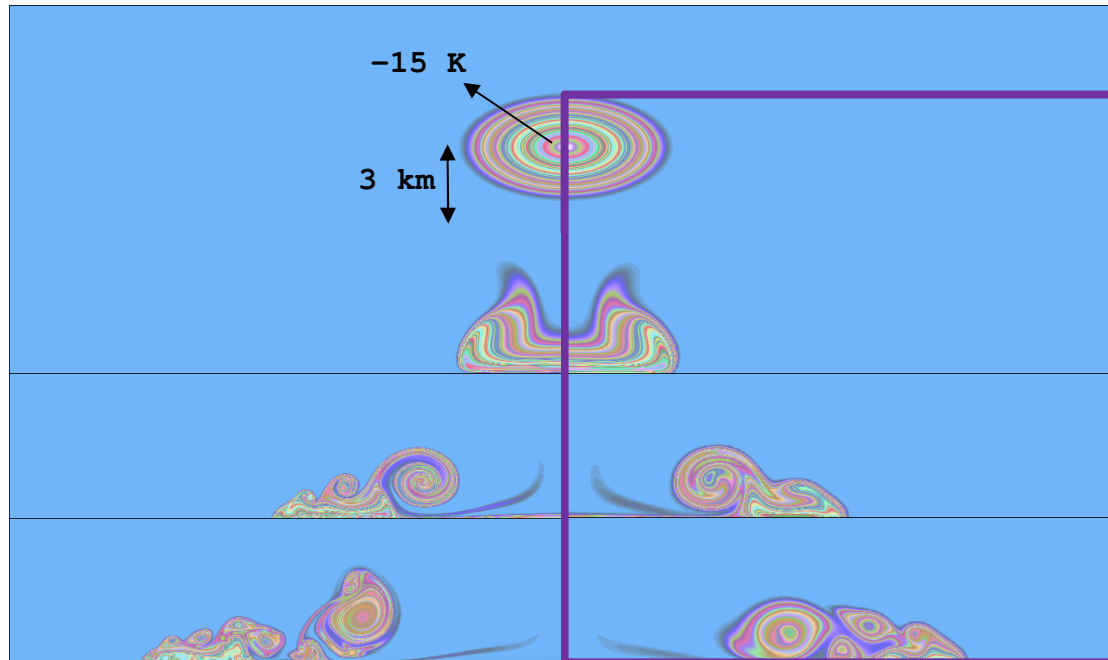
( $dx=dz=100\text{m}$ ,  $dt=0.25\text{s}$ ,  $N_{\text{step}}=10$ , **3h**)

$$\Delta M = -0.46 \%$$

$$\Delta E = -0.56 \%$$

Quadruple resolution

**Initial**

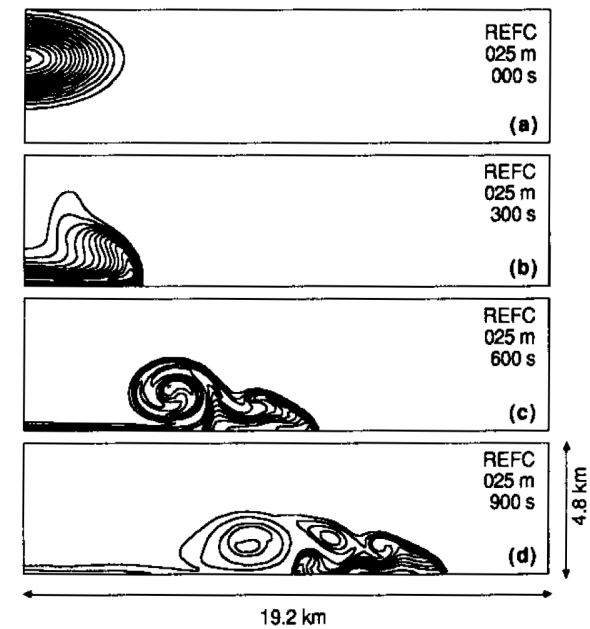


$$\Delta M = -1.6 \%$$

$$\Delta E = -2.0 \%$$

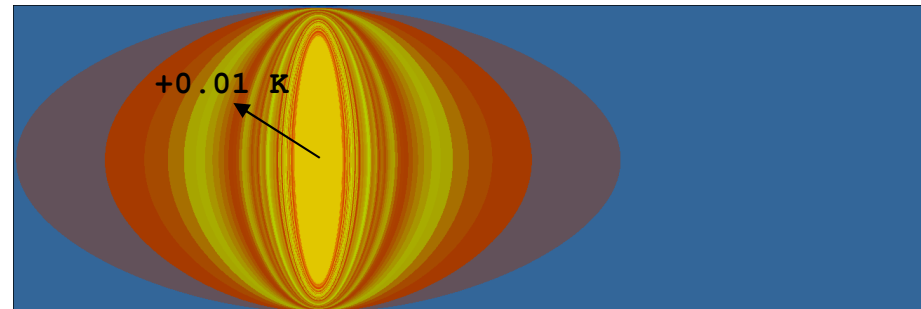


**Straka et al. (1993)**

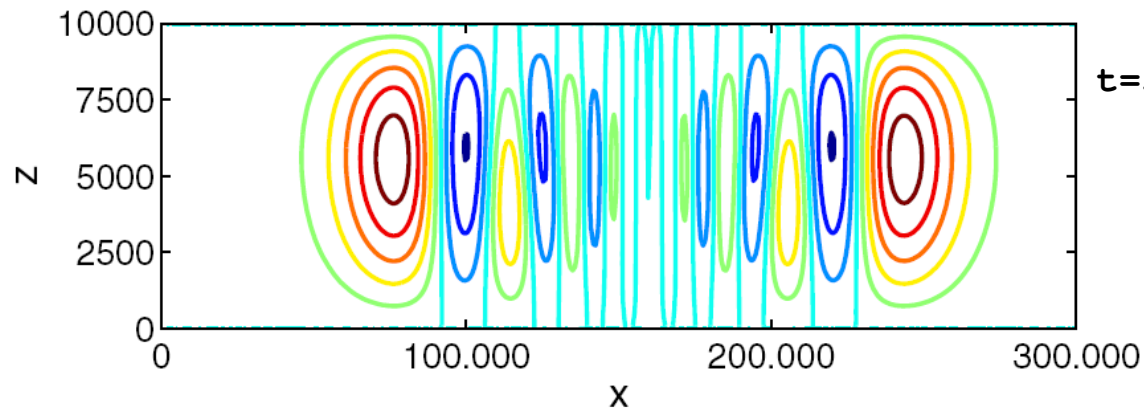


> Inertia-Gravity Waves (uniform wind/stability:  $U=20\text{ms}^{-1}/N=0.01\text{s}^{-1}$ )

( $dx=dz=125\text{m}$ ,  $dt=0.3125\text{s}$ ,  $N_{\text{step}}=10$ , 1h)

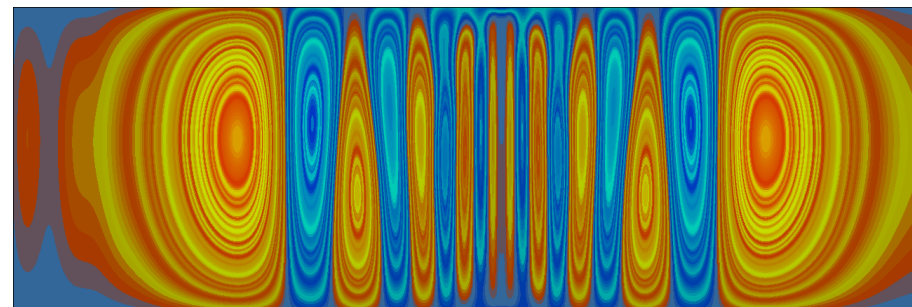


Initial



$t=50\text{min}$

Giraldo  
&  
Restelli  
(2008)



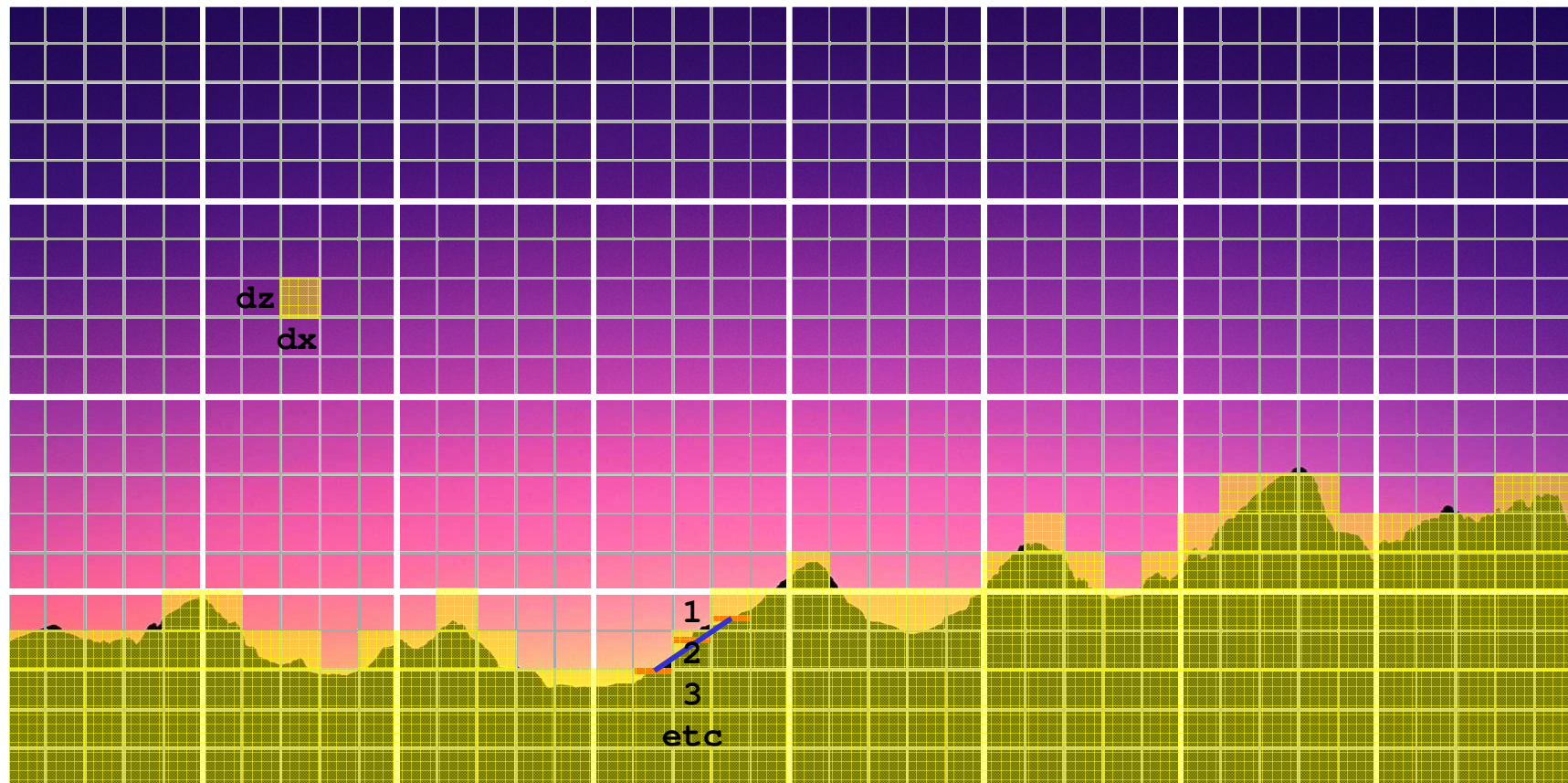
$\Delta M = +0.00001 \%$

$\Delta E = +0.000005 \%$

[Animation](#)

## Inclusion of Orography

- > Use mean terrain height over grid cell



- > Terrain-following Bottom B.C.

Vertical velocity:  $w_2 = (u_1, v_1) \cdot \overrightarrow{slope}$  *Linear extrapolation underneath*

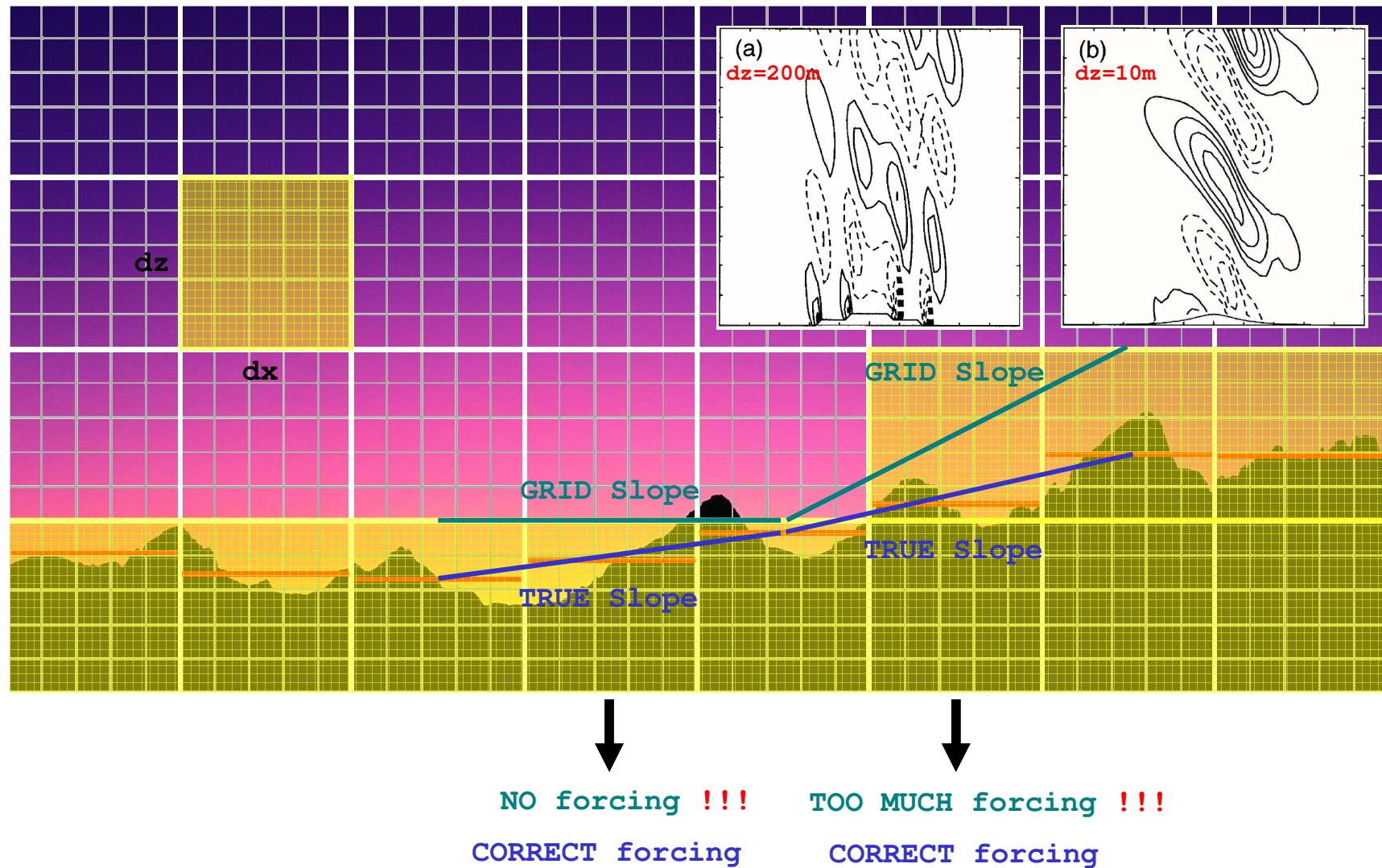
Other fields:  $(u_i, v_i) = (u_1, v_1)$   $(\pi'_i, \theta'_i) = (\pi'_1, 0)$

# Inclusion of Orography

> TRUE-terrain slope **vs** GRID-based slope

ETA MODEL

Gallus & Klemp (2000)

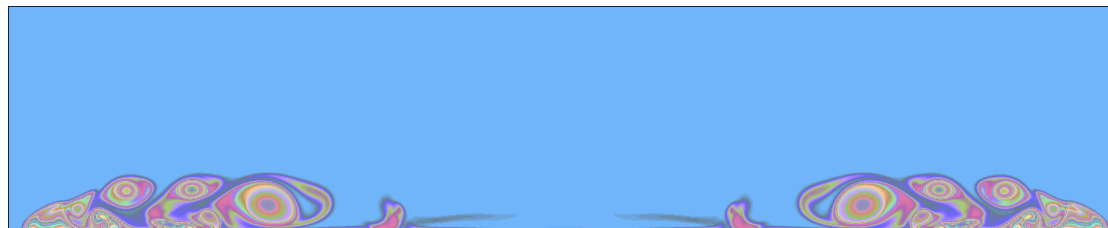
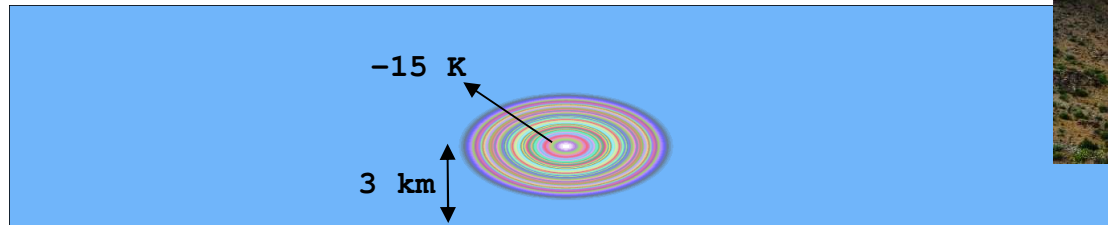




## > Density Current Comparison

(dx=dz=50m, dt=0.125s, Nstep=8, 3h)

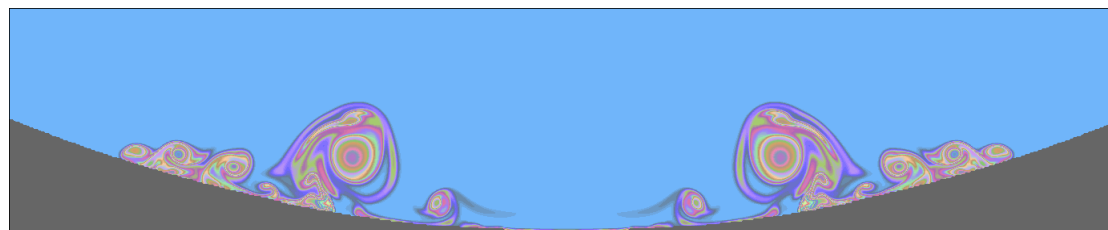
Initial



Flat terrain

$$\Delta M = -0.85 \%$$

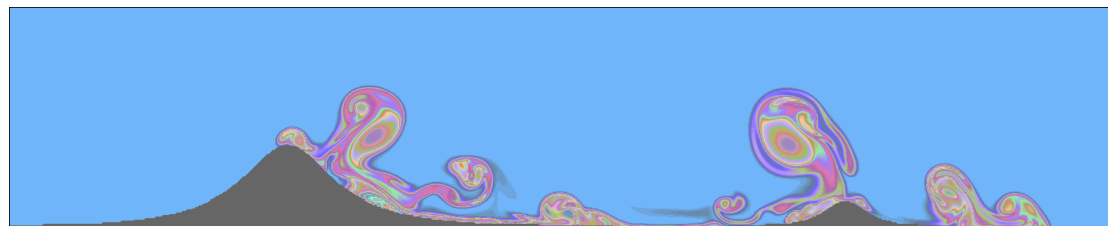
$$\Delta E = -1.06 \%$$



Parabolic slope

$$\Delta M = -0.94 \%$$

$$\Delta E = -1.09 \%$$



Two mountains

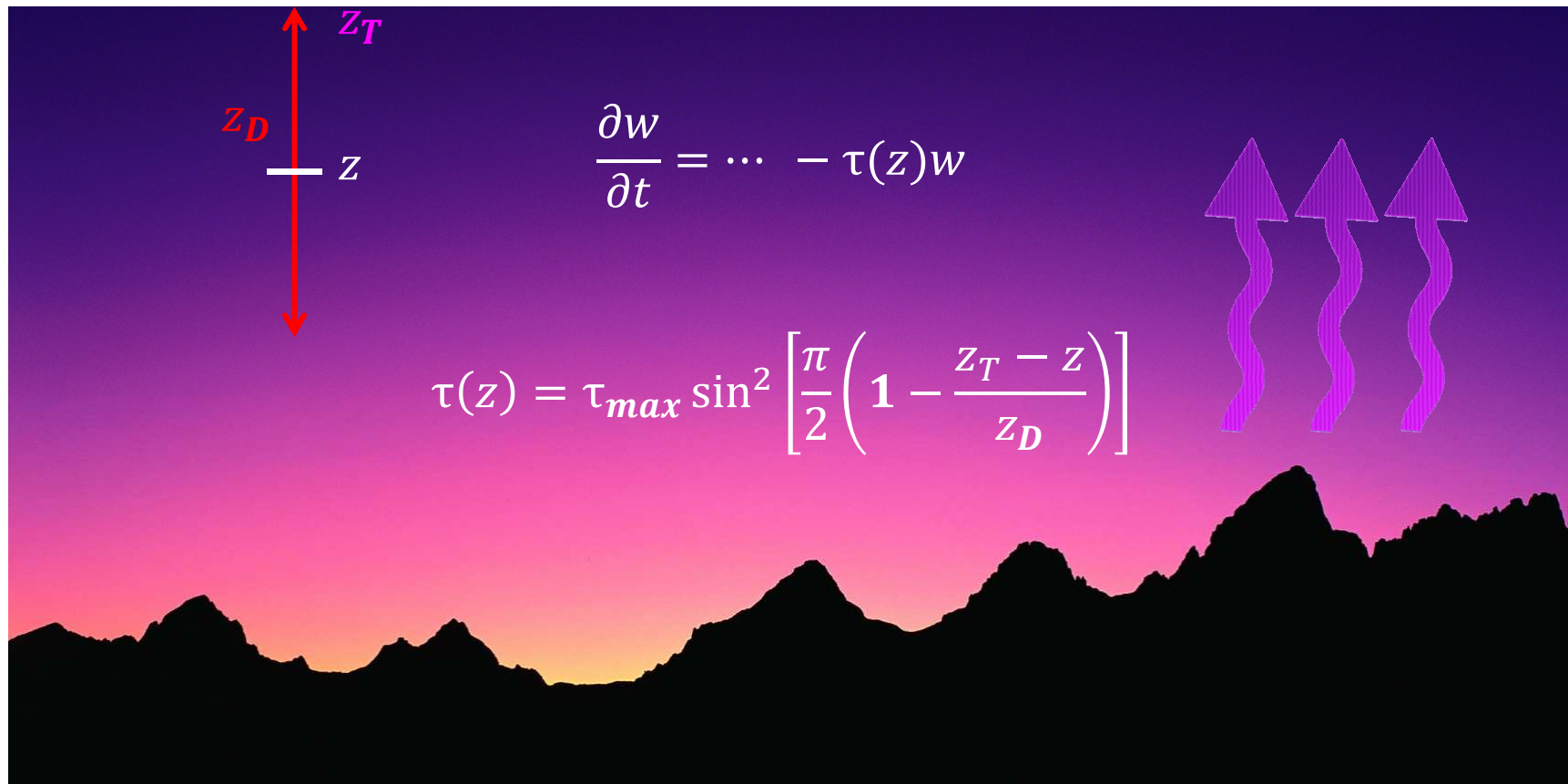
$$\Delta M = +2.26 \%$$

$$\Delta E = +3.12 \%$$

t=21min

## Gravity Wave Absorbing Layer

> Rayleigh damping term added to  $\frac{\partial w}{\partial t}$  equation **within**  $z_D$

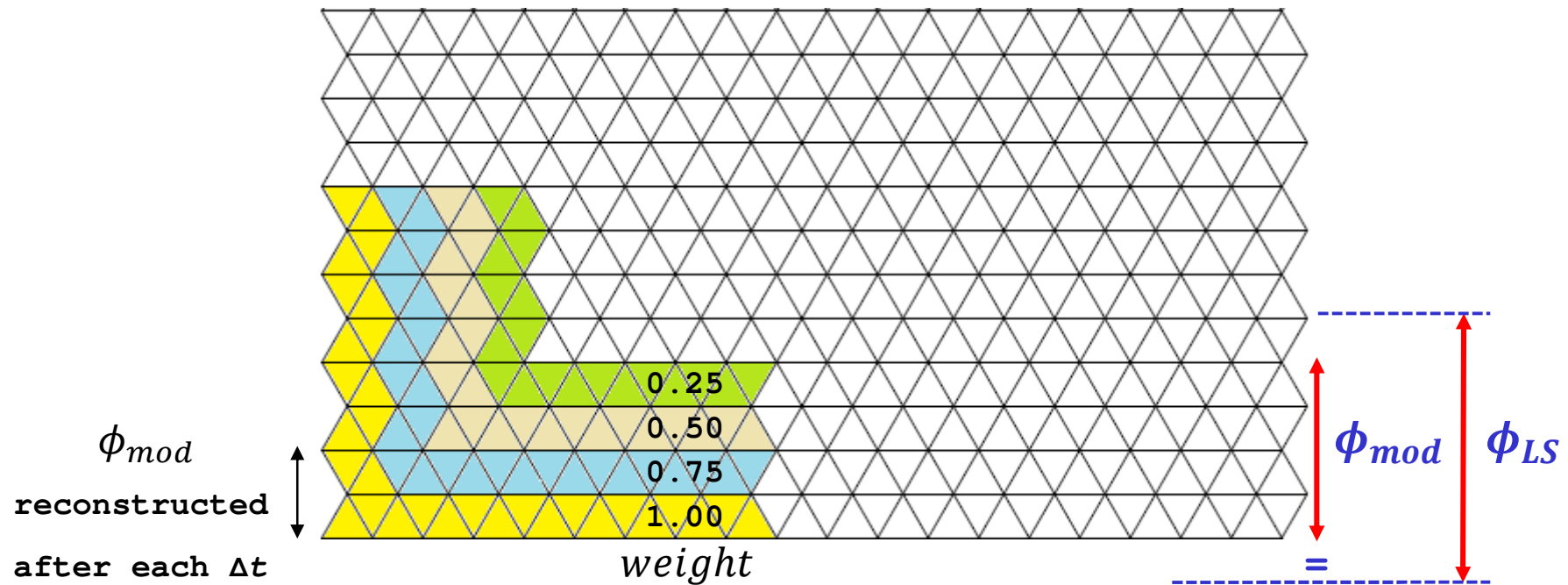


> Typical values  $\begin{cases} z_D = 10 \text{ km} \\ \tau_{max} = 0.1 \text{ s}^{-1} \end{cases}$  (above 10km only)



## Specified Lateral Boundary Conditions

- > Interior solution  $\phi_{mod}$  relaxed towards specified  $\phi_{LS}$

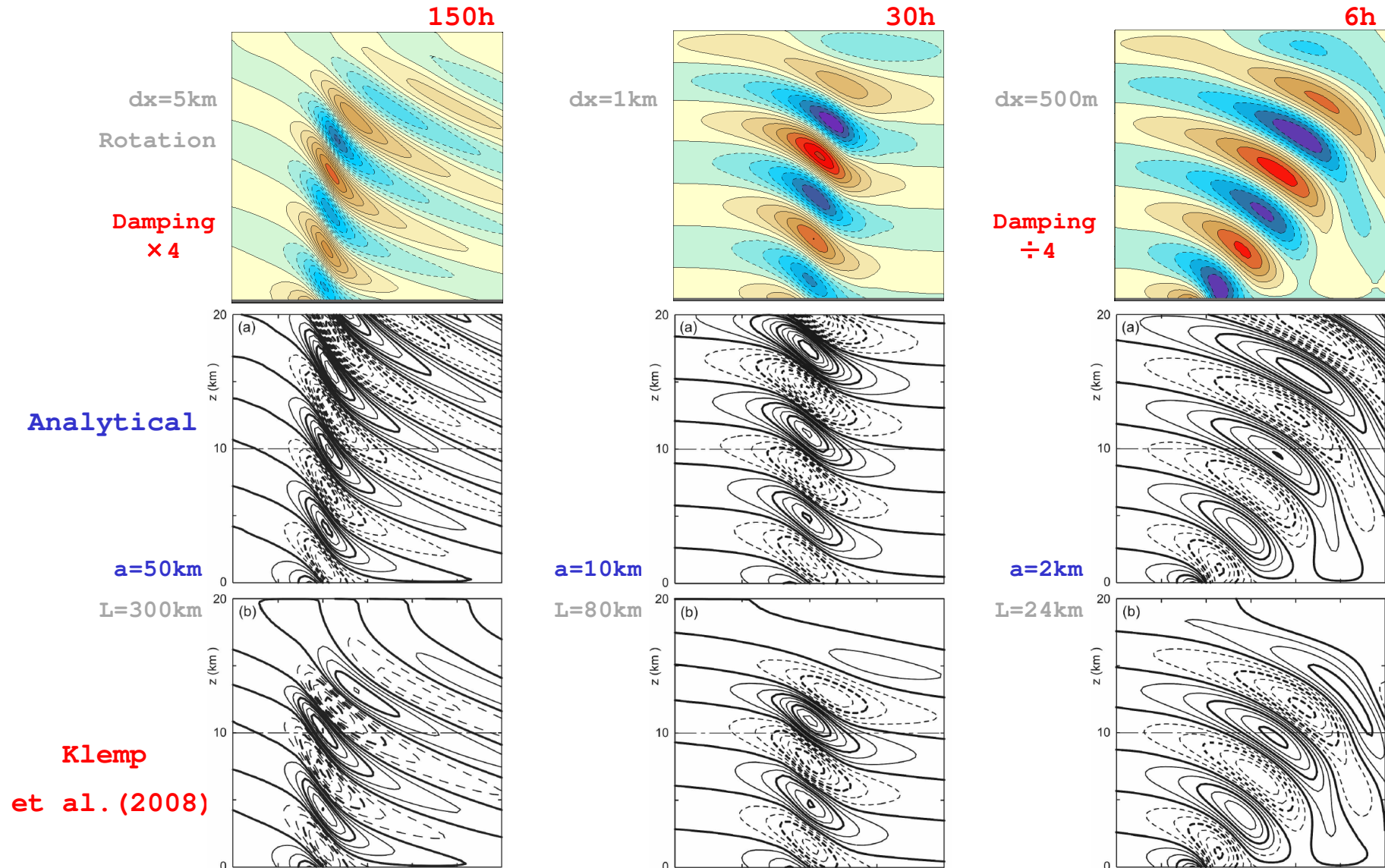


$$\frac{\partial \phi_{mod}}{\partial t} = weight [F(\phi_{LS} - \phi_{mod}) - G\Delta^2(\phi_{LS} - \phi_{mod})]$$

- > Typical values  $\begin{cases} F = 1/10\Delta t \\ G = 1/50\Delta t \end{cases}$  ( $\times 5$  if using grid analyses)

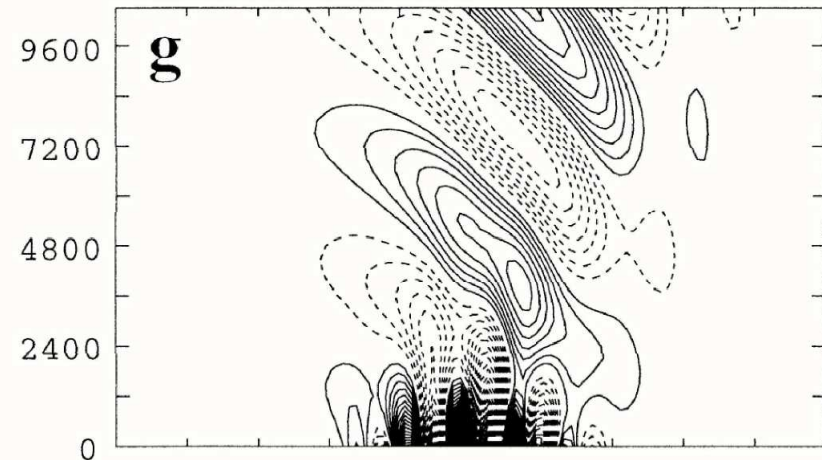
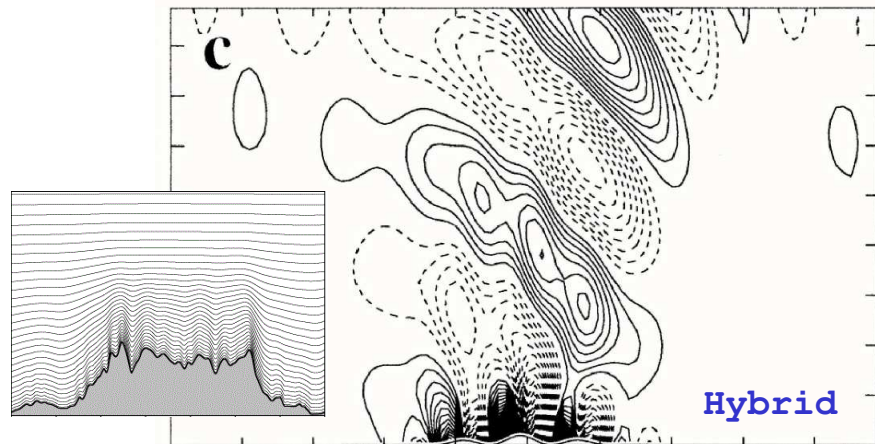
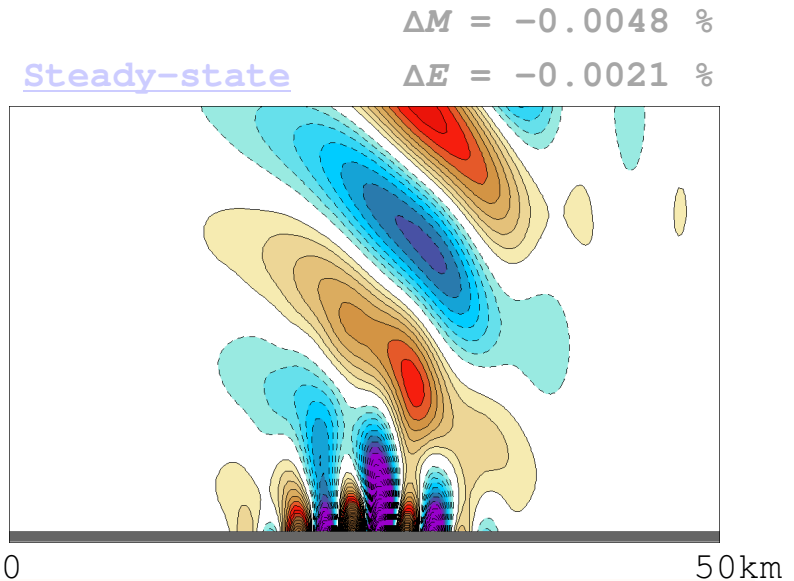
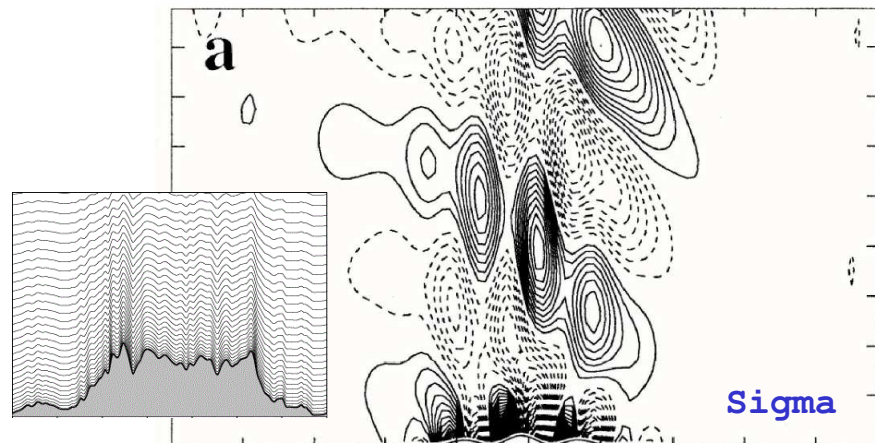
# > Linear Mountain Waves (10m bell-shaped mountain, $U=10\text{ms}^{-1}$ , $N=0.01\text{s}^{-1}$ )

( $dz=200\text{m}$ ,  $dt=0.6\text{s}$ ,  $N\text{step}=10$ )



> **Schär Mountain** (250m bell-shaped + small-scale,  $U=10\text{ms}^{-1}$ ,  $N=0.01\text{s}^{-1}$ )

( $dx=250\text{m}$ ,  $dz=250\text{m}$ ,  $dt=0.75\text{s}$ ,  $N_{\text{step}}=10$ , 10h)



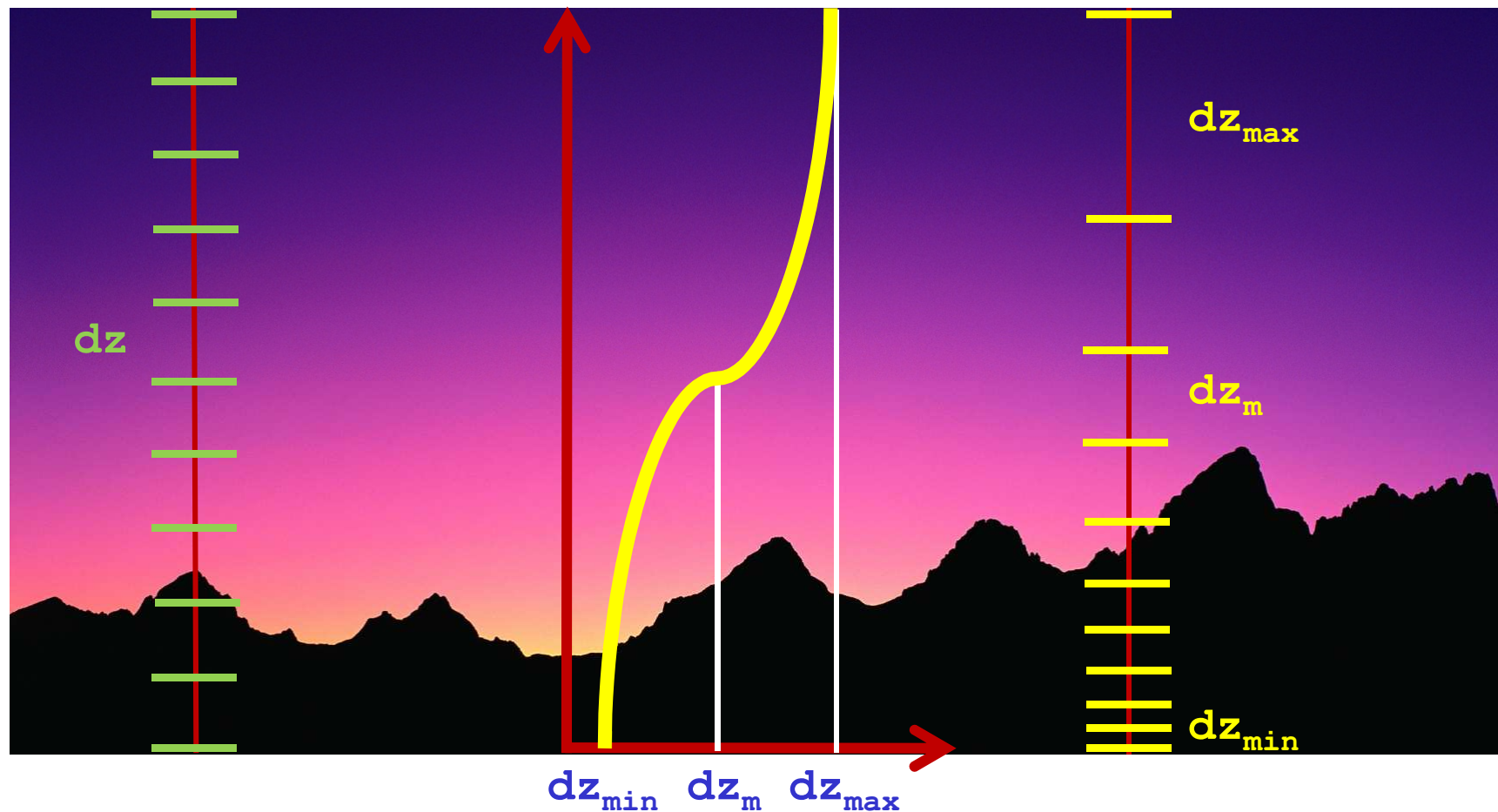
Schär et al. (2002)

Analytical



## Vertical Stretching

- > Higher resolution at low levels (cos profile)



- > Two parameters (stretch,  $dz_m$ ) 
$$\begin{cases} dz_{min} = dz_m / stretch \\ dz_{max} = dz_m + (dz_m - dz_{min}) \end{cases}$$

## > Stabilization of acoustic vertical modes (RK2-cycle)

$$\frac{\partial \pi'}{\partial t} = F^n + G^n \left[ \alpha \frac{\partial w^n}{\partial z} + \beta \frac{\partial w^{n+1}}{\partial z} \right] \longrightarrow \pi'^{n+1} = A + B \frac{\partial w^{n+1}}{\partial z}$$

$$\frac{\partial w}{\partial t} = R^n + T^n \left[ \alpha \frac{\partial \pi'^n}{\partial z} + \beta \frac{\partial \pi'^{n+1}}{\partial z} \right] \longrightarrow w^{n+1} = C + D \frac{\partial \pi'^{n+1}}{\partial z}$$

$$\alpha=0.3 \quad \beta=0.7$$

Off-centered

$$w^{n+1} = C + DA_z + DB_z \frac{\partial w^{n+1}}{\partial z} + DB \frac{\partial^2 w^{n+1}}{\partial z^2}$$

$$aw_{k-1}^{n+1} + bw_k^{n+1} + cw_{k+1}^{n+1} = f \xrightarrow{\text{Tridiagonal solver}} \begin{cases} w^{n+1} \\ \pi'^{n+1} \end{cases} \xrightarrow{\text{F-B}} u^{n+1}, v^{n+1}$$

## > Additional optimizations [CFL $\xrightarrow{c_s > 300 \text{ m/s}} \Delta t \approx 2 \Delta x (\Delta z)$ ]

\* Vertical diffusion implicit (BTCS/CN)

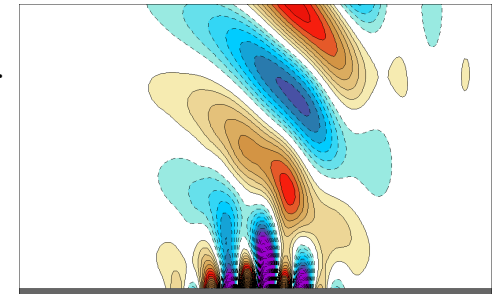
\* Slow terms and  $\theta'$  in Nsteps-cycle

\* Flexible REA-V

## > Schär Mountain Comparison

(dx=250m, dzm=250m, dt=0.75s, Nstep=10, 10h)

stretch=1

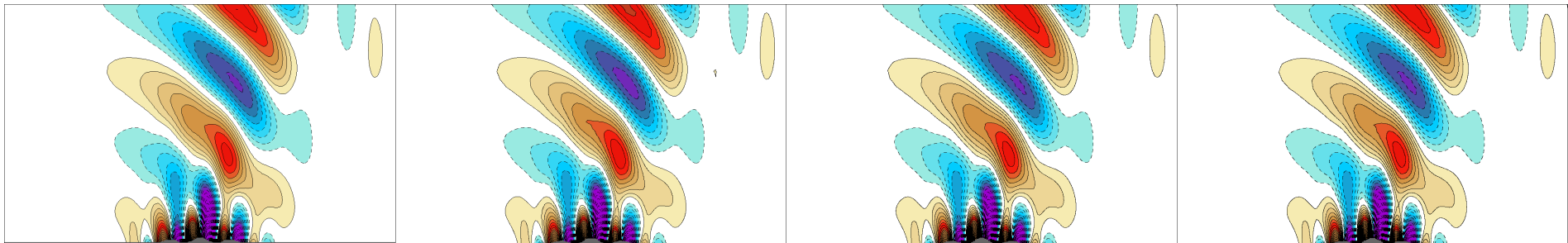


stretch=5

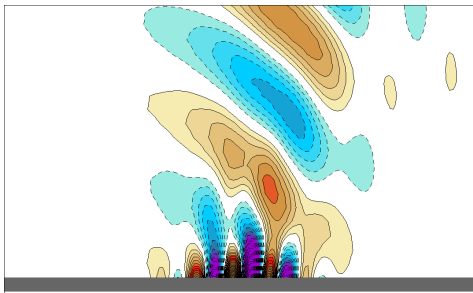
stretch=10

stretch=20

stretch=30

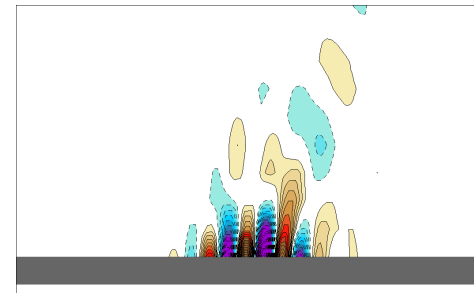


dzm=500m

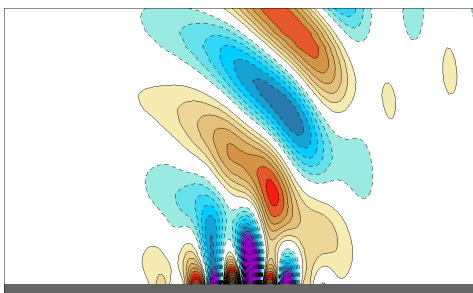


stretch=1

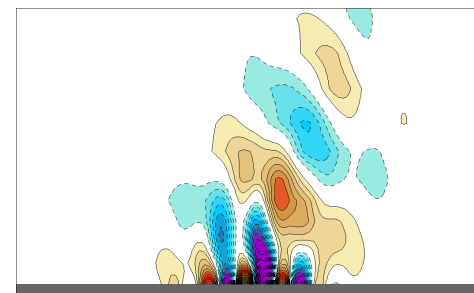
dzm=1000m



stretch=1



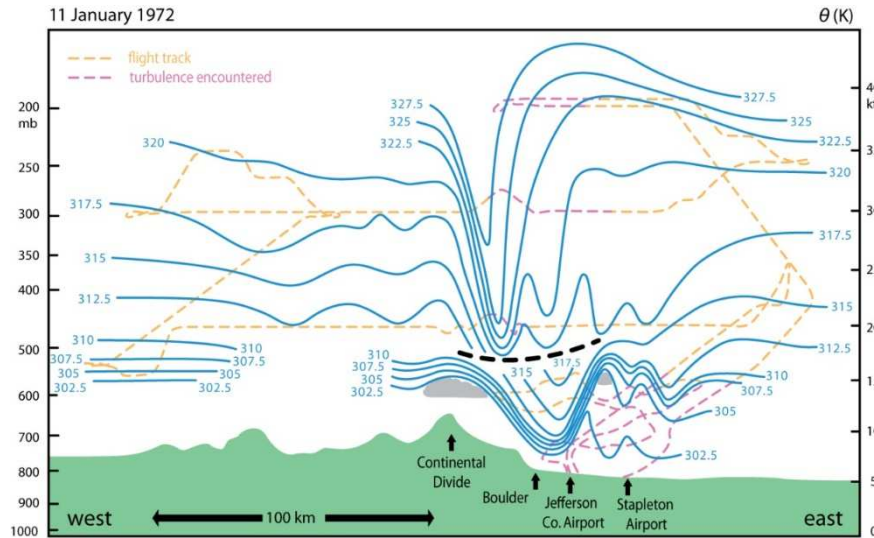
stretch=2



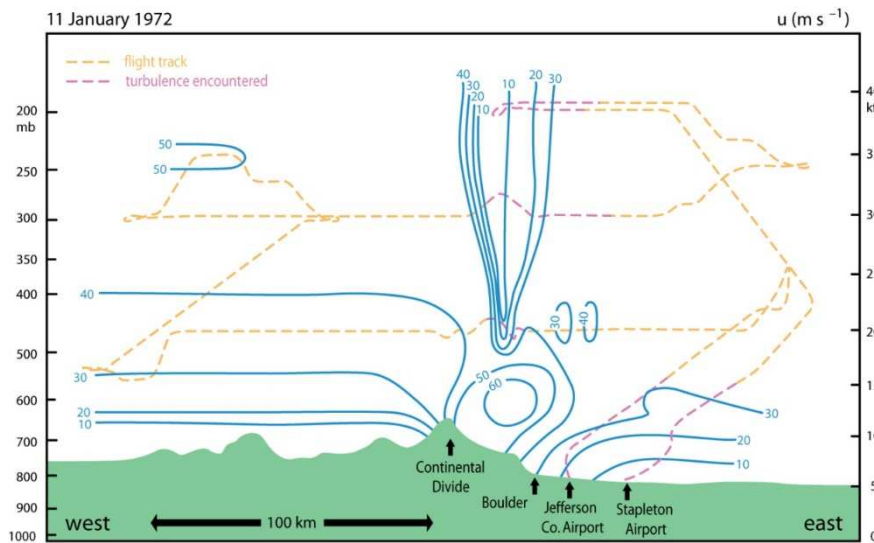
stretch=4



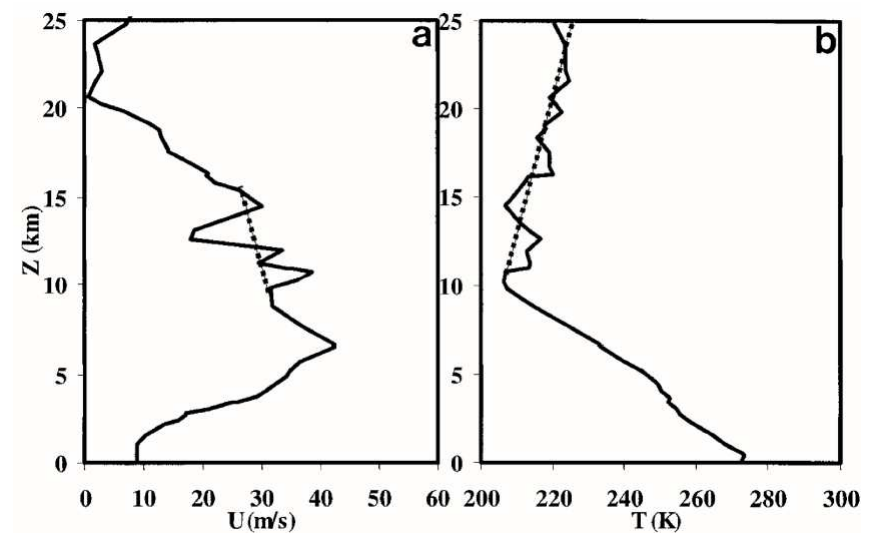
## > 11 January 1972 Boulder Windstorm



Klemp and Lilly (1975)



Grand Junction, CO  
sounding at 12 UTC

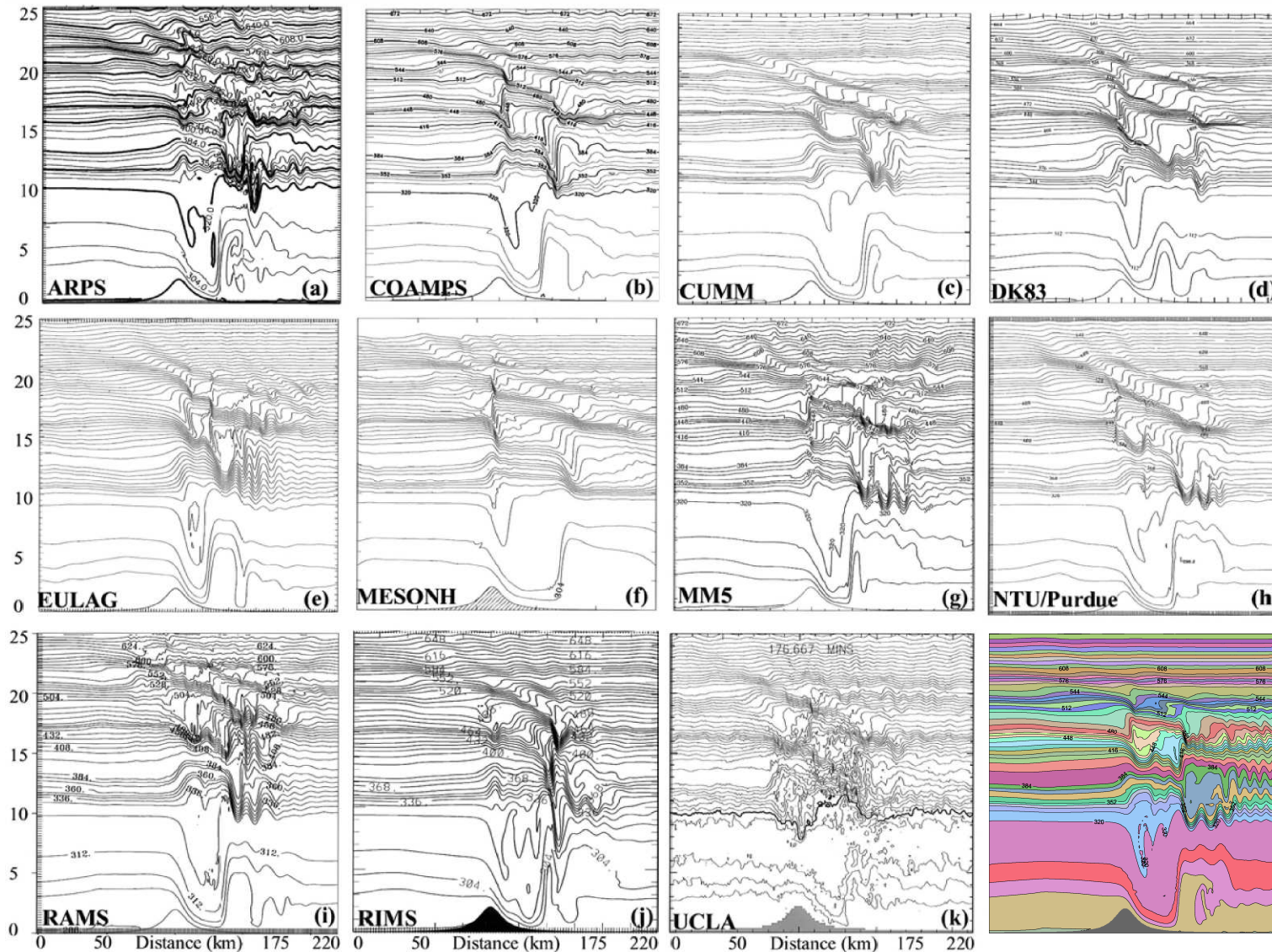


# > 11 January 1972 Boulder Windstorm

(dx=500m, dzm=125m, stretch=5, dt=1.5s, Nstep=8, 20h)

t=3h

Doyle et al.  
(2000)



TRAM

$$\Delta M = -0.76 \%$$

$$\Delta E = -0.36 \%$$

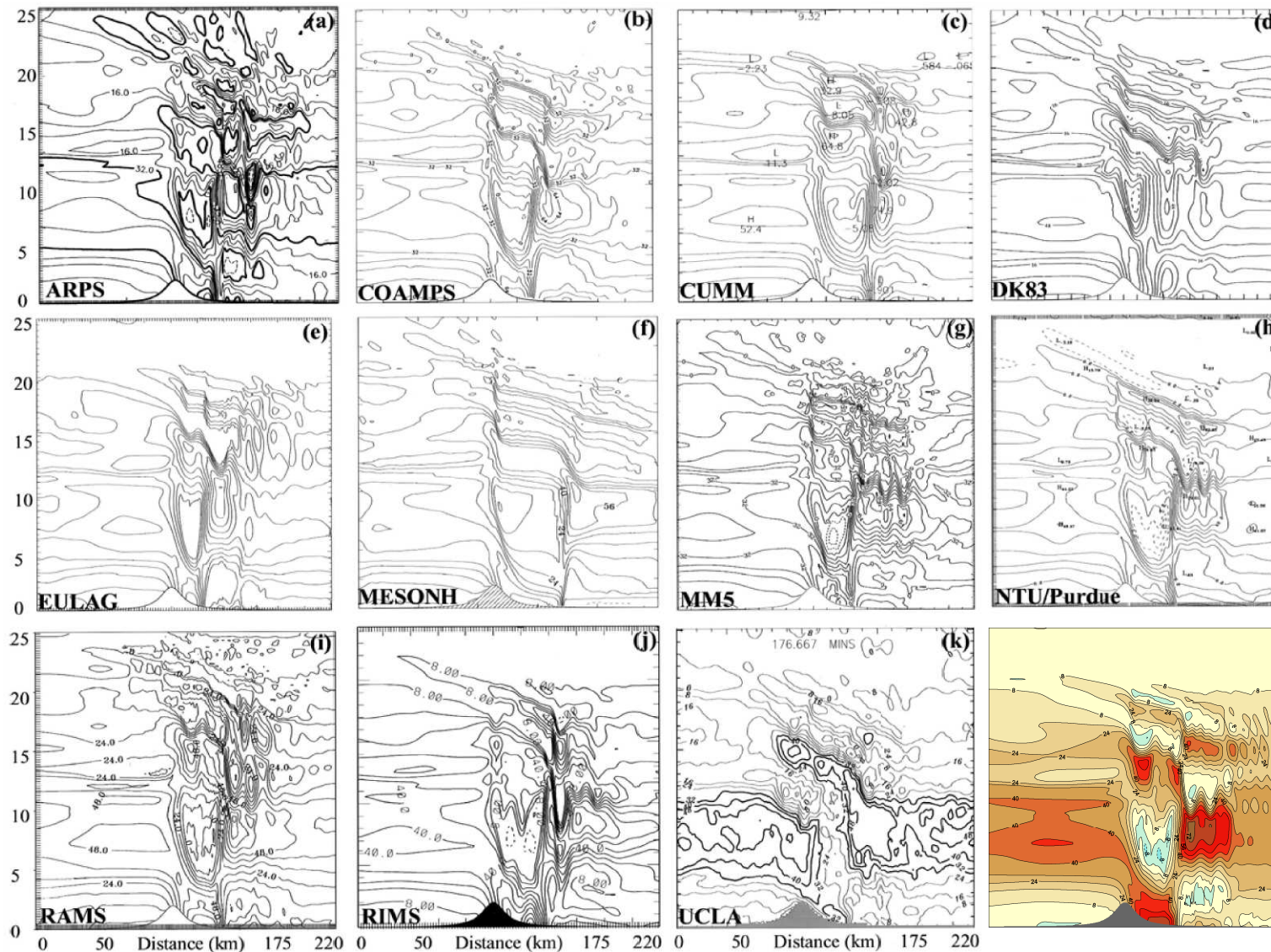


# > 11 January 1972 Boulder Windstorm

(dx=500m, dzm=125m, stretch=5, dt=1.5s, Nstep=8, 20h)

t=3h

Doyle et al.  
(2000)

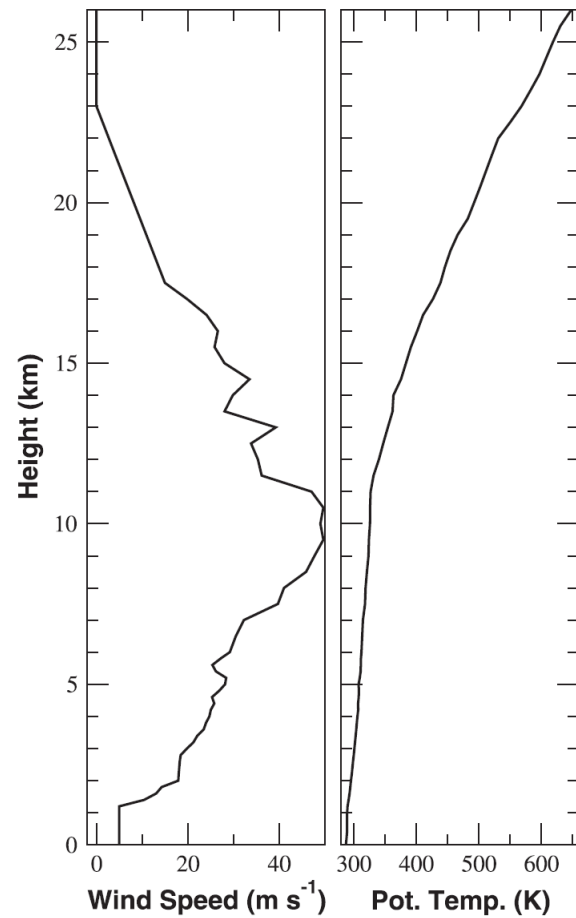


TRAM

$$\Delta M = -0.76 \%$$

$$\Delta E = -0.36 \%$$

> T-REX Intense Mountain-Wave



21 UTC 25 Mar 2006  
Sounding upstream of the  
Sierra Nevada (CA)



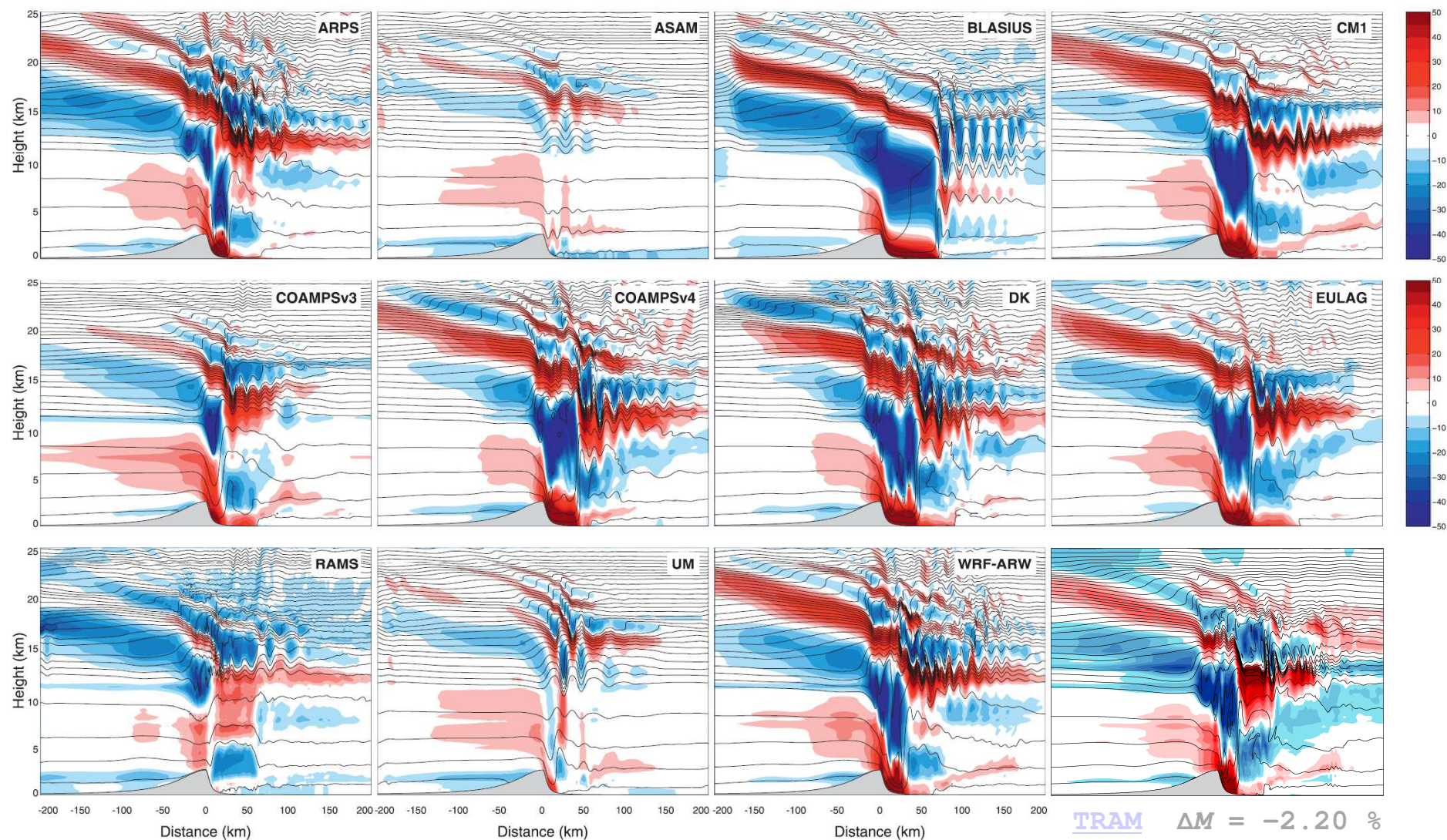


> T-REX Intense Mountain-Wave

t=4h

(dx=500m, dzm=100m, stretch=5, dt=1.5s, Nstep=6, 20h)

Doyle et al. (2011)

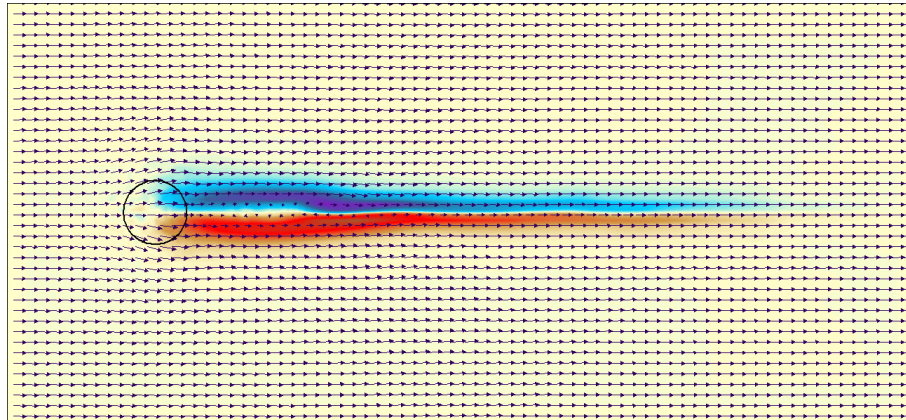




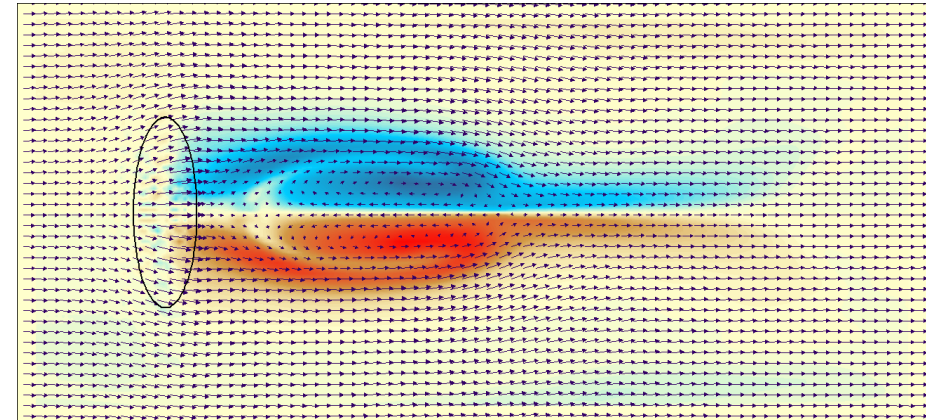
> Vortices Past Isolated Topography ( $U=10\text{ms}^{-1}$ ,  $N=0.01\text{s}^{-1}$ )

( $dx=2\text{km}$ ,  $dzm=500\text{m}$ ,  $stretch=2$ ,  $dt=4\text{s}$ ,  $Nstep=10$ , 48h)

e.g. Schär and Durran (1997)

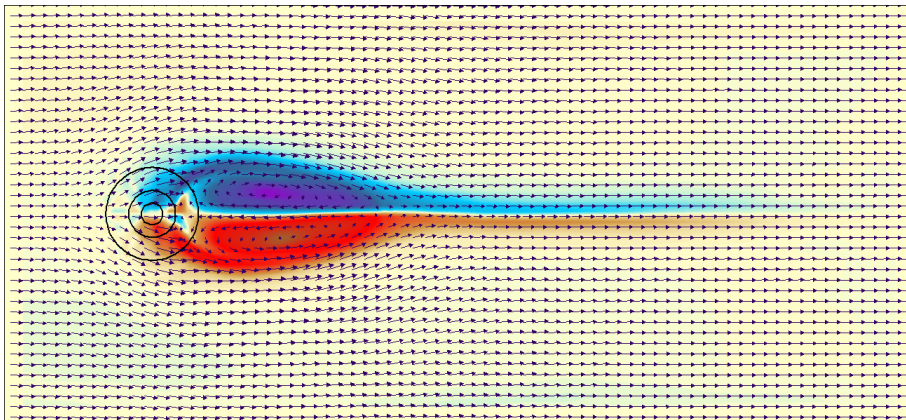


h=1500m

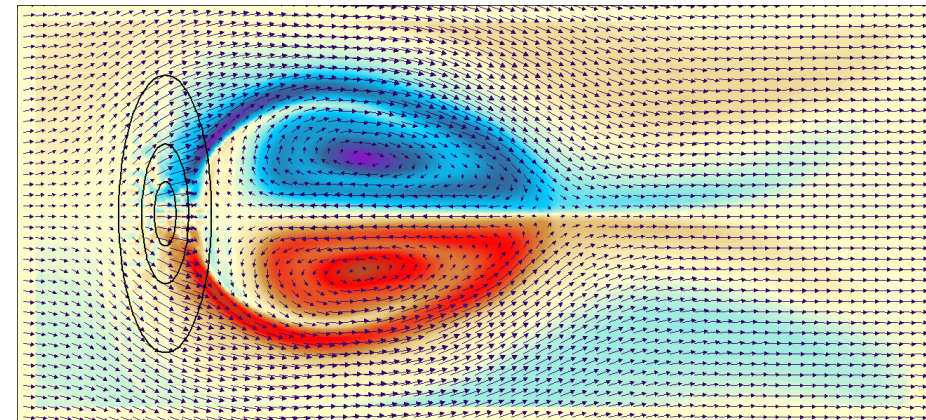


h=1500m

t=6h



h=3000m



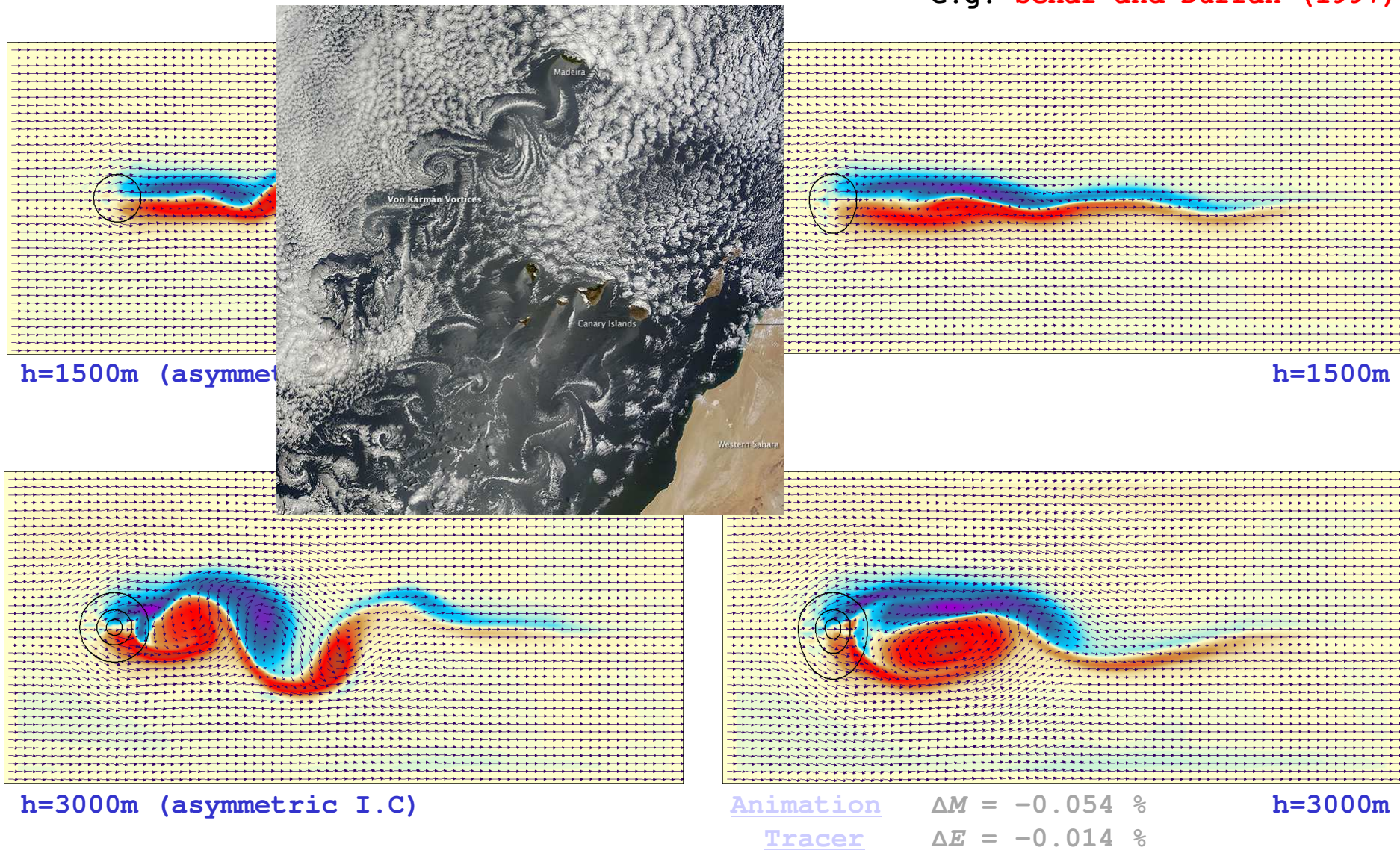
h=3000m



# > Von Kármán Vortex Streets ( $U=10\text{ms}^{-1}$ , $N=0.01\text{s}^{-1}$ )

( $dx=2\text{km}$ ,  $dzm=500\text{m}$ ,  $stretch=2$ ,  $dt=4\text{s}$ ,  $Nstep=10$ , 48h)

e.g. Schär and Durran (1997)



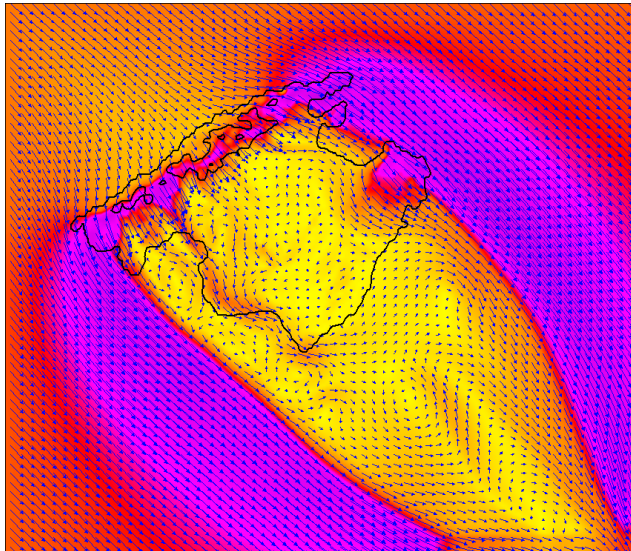


> Idealized Flow over Mallorca ( $U=5\text{ms}^{-1}$ ,  $N=0.0184\text{s}^{-1}$ )

( $dx=1.5\text{km}$ ,  $dzm=400\text{m}$ ,  $stretch=20$ ,  $dt=3\text{s}$ ,  $Nstep=10$ , 24h)

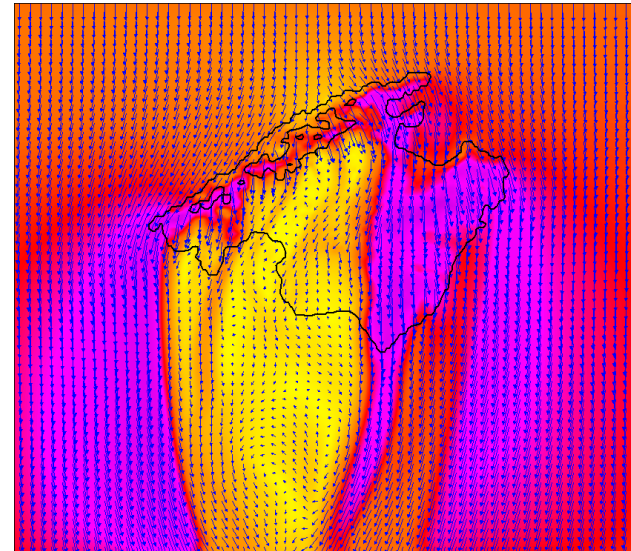
$\Delta M < 0.015 \%$   $\Delta E < 0.0004 \%$

Northwest

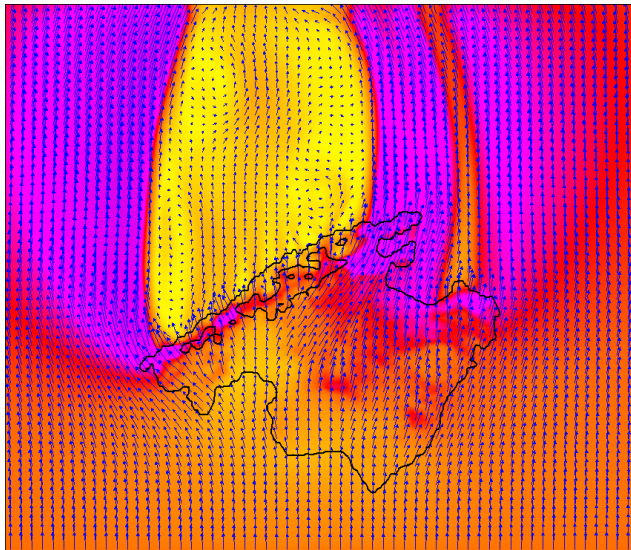


t=24h

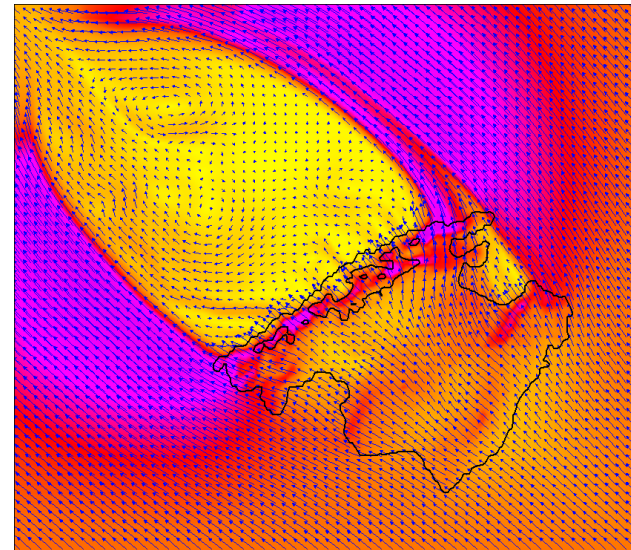
North



South



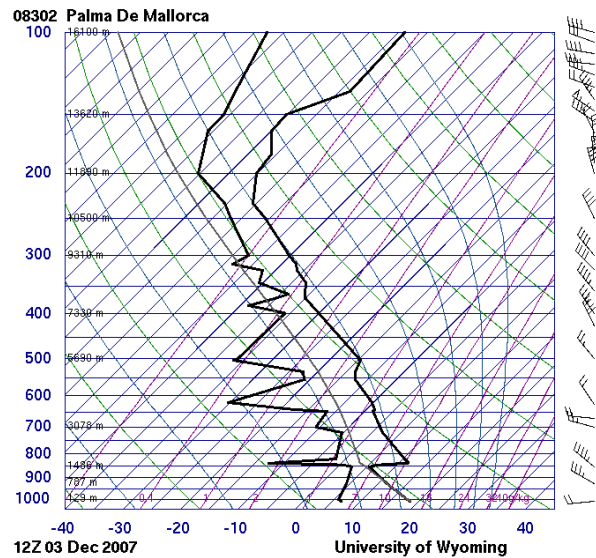
Southeast



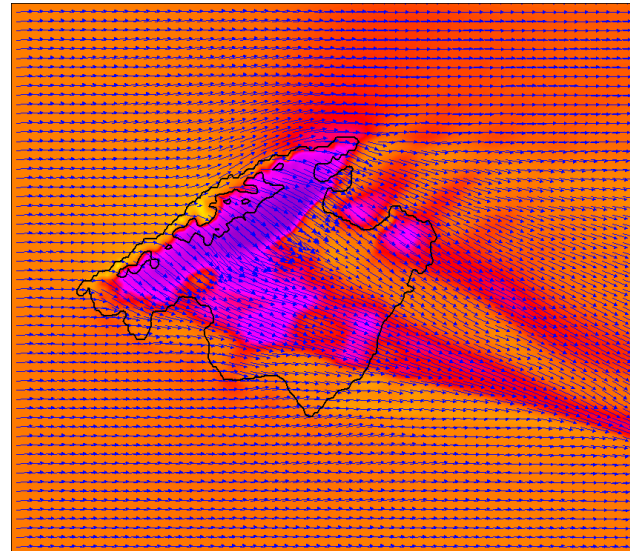
## > Sounding-Derived Flow over Mallorca

(dx=1.5km, dzm=400m, stretch=20, dt=3s, Nstep=10, 24h)

t=12h

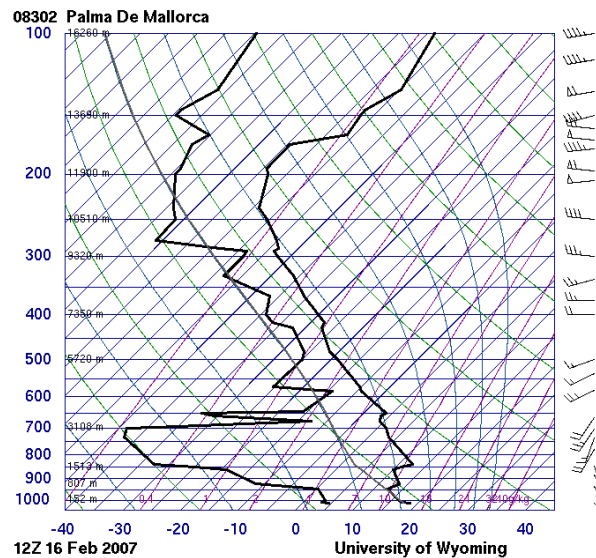


Run

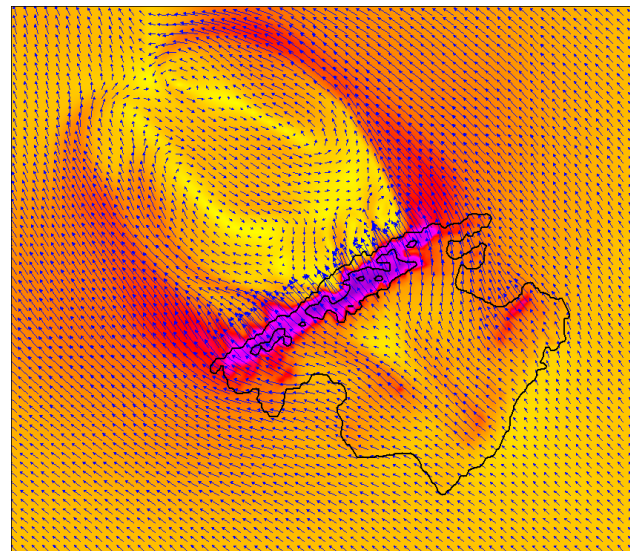


$$\Delta M = -0.059 \%$$

$$\Delta E = +0.0030 \%$$



Run



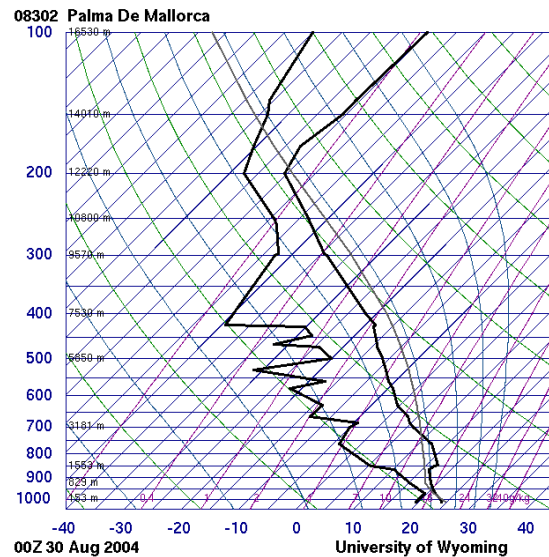
$$\Delta M = -0.027 \%$$

$$\Delta E = +0.0001 \%$$

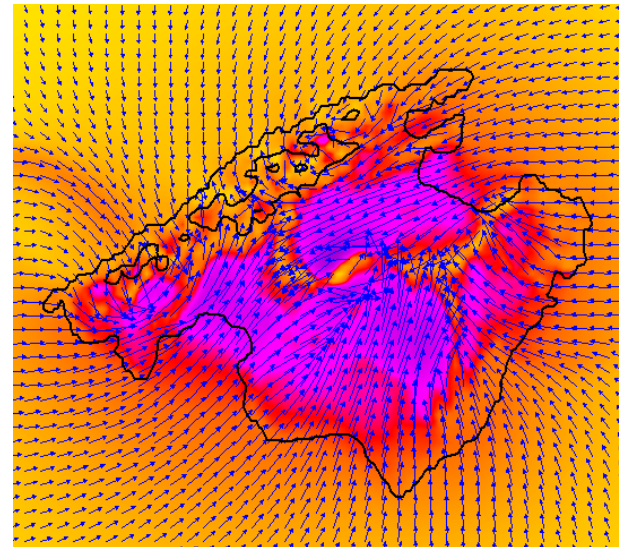


# > Breeze Circulation in Mallorca ( $\theta'_s$ , Diffusion $\theta'$ , Coriolis)

(dx=1.5km, dzm=400m, stretch=20, dt=3s, Nstep=10, 24h)



Run



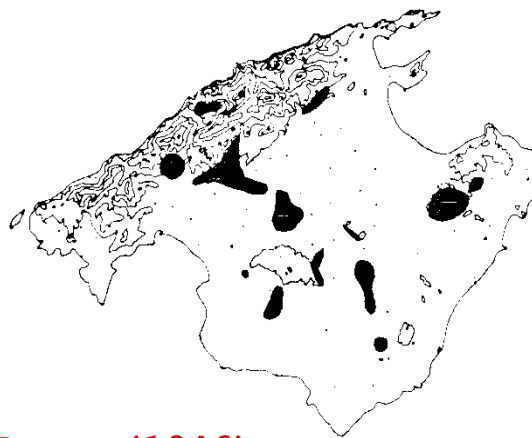
t=13h

$\Delta M = -0.0013 \%$

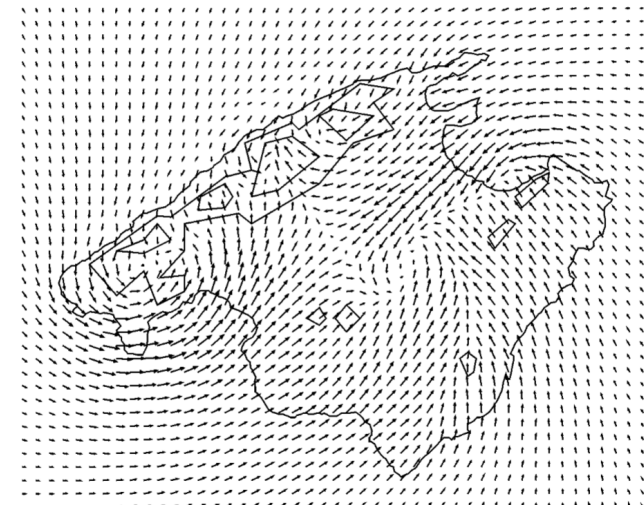
$\Delta E = +0.00007 \%$



Jansà & Jaume (1946)



Ramis & Romero (1995)



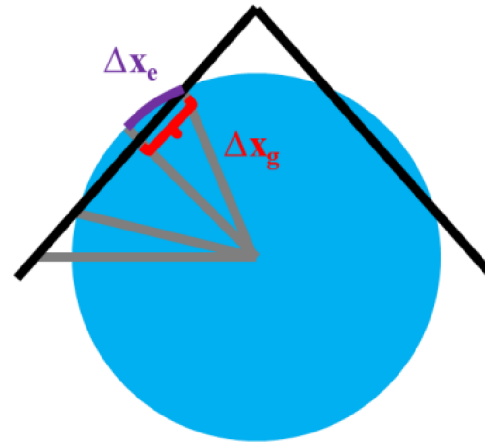


# Real Case Applications

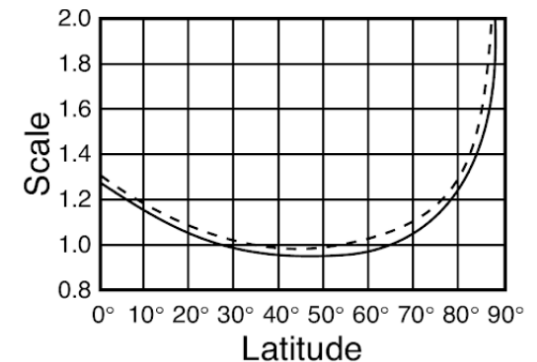
> Lambert conformal map projection

+ Coriolis terms

+ Curvature terms



$$m = \frac{\Delta x_g}{\Delta x_e}$$



> Modified equations

$$\frac{\partial \pi'}{\partial t} = -mu \frac{\partial \pi'}{\partial x} - mv \frac{\partial \pi'}{\partial y} - w \frac{\partial \pi'}{\partial z} - w \frac{\partial \bar{\pi}}{\partial z} - \frac{R}{c_v} (\bar{\pi} + \pi') \left[ m^2 \frac{\partial (\frac{u}{m})}{\partial x} + m^2 \frac{\partial (\frac{v}{m})}{\partial y} + \frac{\partial w}{\partial z} \right]$$

$$\frac{\partial \theta'}{\partial t} = -mu \frac{\partial \theta'}{\partial x} - mv \frac{\partial \theta'}{\partial y} - w \frac{\partial \theta'}{\partial z} - w \frac{\partial \bar{\theta}}{\partial z} \quad [\text{Diffusion terms omitted}]$$

$$\frac{\partial u}{\partial t} = -mu \frac{\partial u}{\partial x} - mv \frac{\partial u}{\partial y} - w \frac{\partial u}{\partial z} - c_p (\bar{\theta} + \theta') m \frac{\partial \pi'}{\partial x} + v \left( f + u \frac{\partial m}{\partial y} - v \frac{\partial m}{\partial y} \right) - \hat{f} w \cos \alpha - \frac{uw}{a}$$

$$\frac{\partial v}{\partial t} = -mu \frac{\partial v}{\partial x} - mv \frac{\partial v}{\partial y} - w \frac{\partial v}{\partial z} - c_p (\bar{\theta} + \theta') m \frac{\partial \pi'}{\partial y} - u \left( f + u \frac{\partial m}{\partial y} - v \frac{\partial m}{\partial y} \right) + \hat{f} w \sin \alpha - \frac{vw}{a}$$

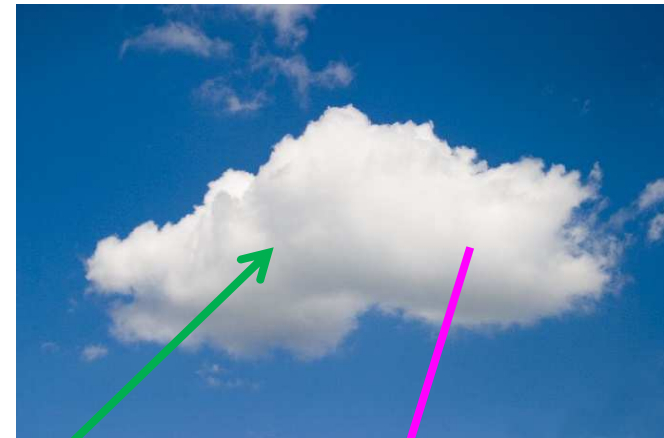
$$\frac{\partial w}{\partial t} = -mu \frac{\partial w}{\partial x} - mv \frac{\partial w}{\partial y} - w \frac{\partial w}{\partial z} - c_p (\bar{\theta} + \theta') \frac{\partial \pi'}{\partial z} + g \frac{\theta'}{\bar{\theta}} + \hat{f} (u \cos \alpha - v \sin \alpha) + \frac{u^2 + v^2}{a}$$

# Simple Representation of Moist Processes

## > Equations for Water Vapor/Cloud Water Mixing Ratios

$$\frac{\partial r_v}{\partial t} = -mu \frac{\partial r_v}{\partial x} - mv \frac{\partial r_v}{\partial y} - w \frac{\partial r_v}{\partial z} - \dot{r}_{cond} + \dot{r}_{evap}$$

$$\frac{\partial r_c}{\partial t} = -mu \frac{\partial r_c}{\partial x} - mv \frac{\partial r_c}{\partial y} - w \frac{\partial r_c}{\partial z} + \dot{r}_{cond} - \dot{r}_{evap}$$



## > WV $\Leftrightarrow$ CW Parameterization

Rutledge & Hobbs (1983):

$$\dot{r}_{cond} \equiv \frac{r_v - r_{vsat}}{\Delta t \left( 1 + \frac{L_v^2 r_{vsat}}{c_p R_v T^2} \right)}$$

$$\dot{r}_{evap} \equiv \frac{r_{vsat} - r_v}{\Delta t \left( 1 + \frac{L_v^2 r_{vsat}}{c_p R_v T^2} \right)}$$

$$r_v > r_{vsat}$$

$$r_c > 0$$

$$r_{vsat} > r_v$$

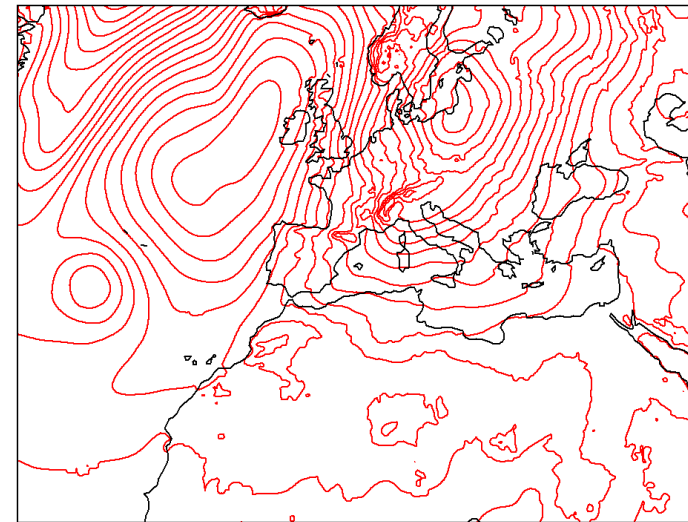
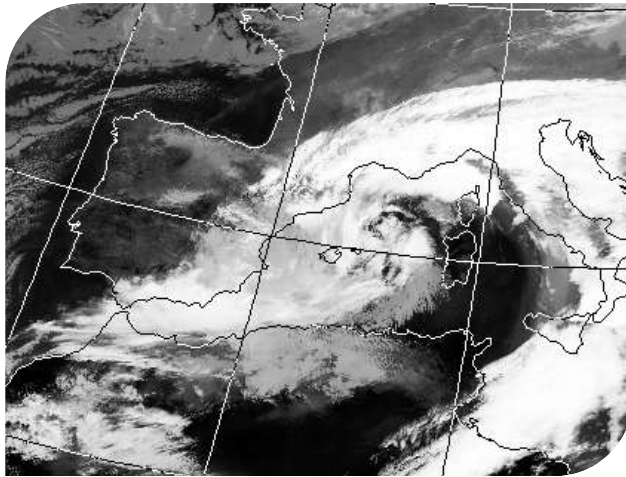
## > NO Precipitation & NO Feedback on Thermodynamics

EXAMPLE: T-REX with RH=90%

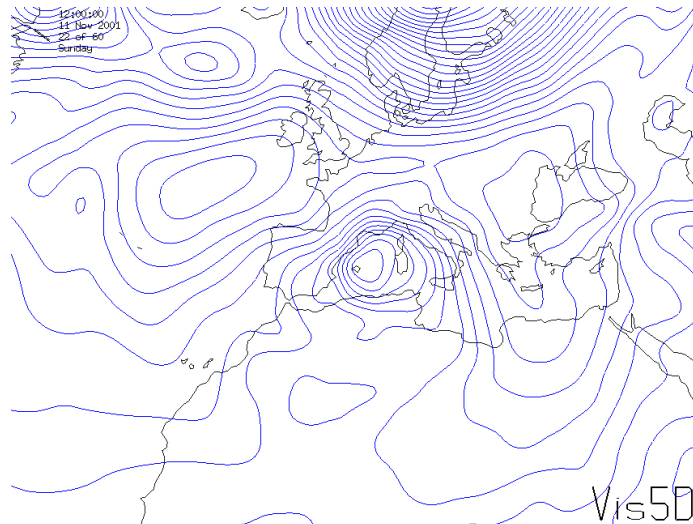
> "SUPERSTORM" Baroclinic Cyclone (IC: 00 UTC 9 Nov 2001)

(dx=50km, dzm=200m, stretch=1, dt=75s, Nstep=6, 120h)

$\Delta M = +0.056 \%$   $\Delta E = +0.071 \%$

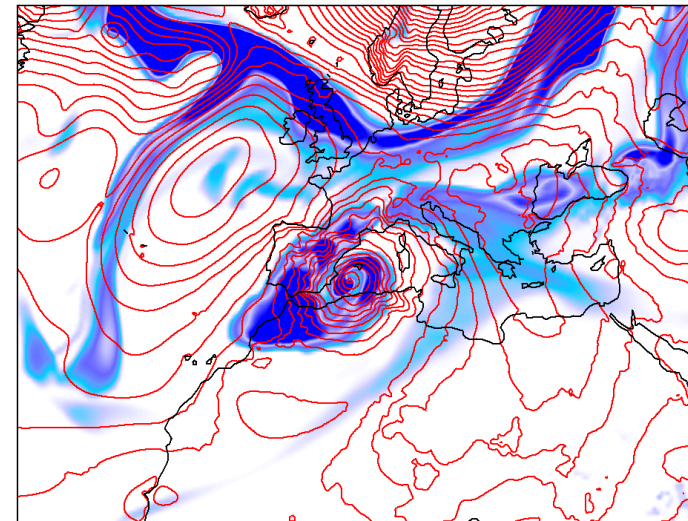


Initial



NCEP

t=60h

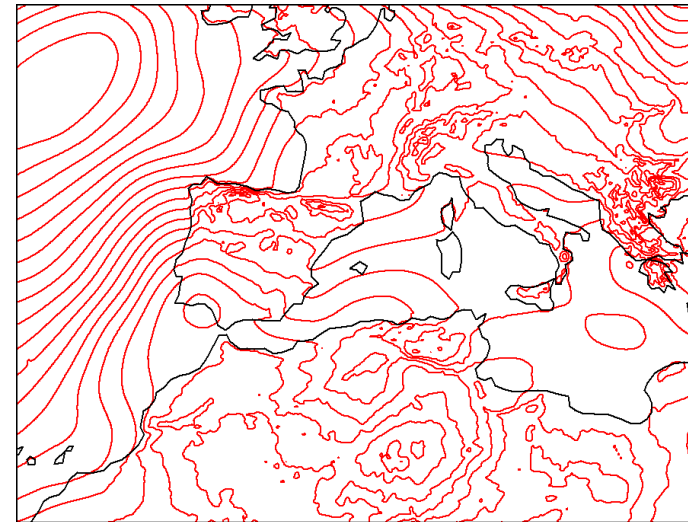
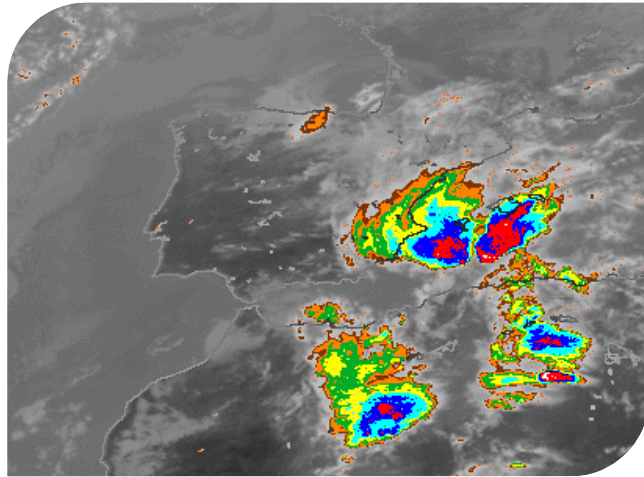


TRAM

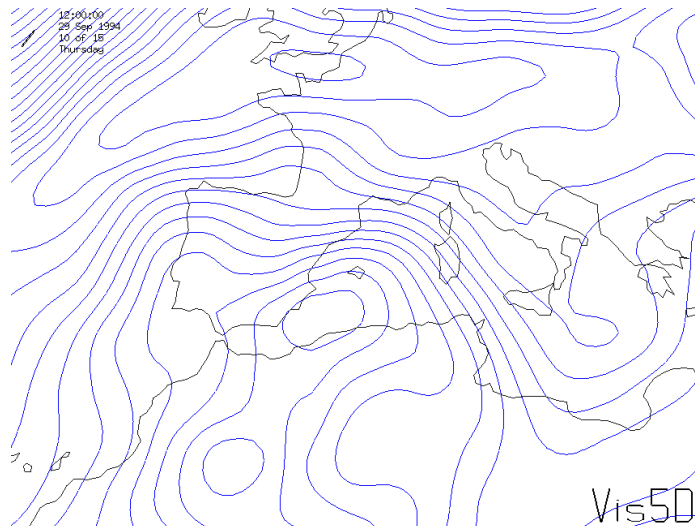
> "VALENCIA" Flood Episode (IC: 00 UTC 28 Sept 1994)

(dx=25km, dzm=200m, stretch=10, dt=40s, Nstep=6, 96h)

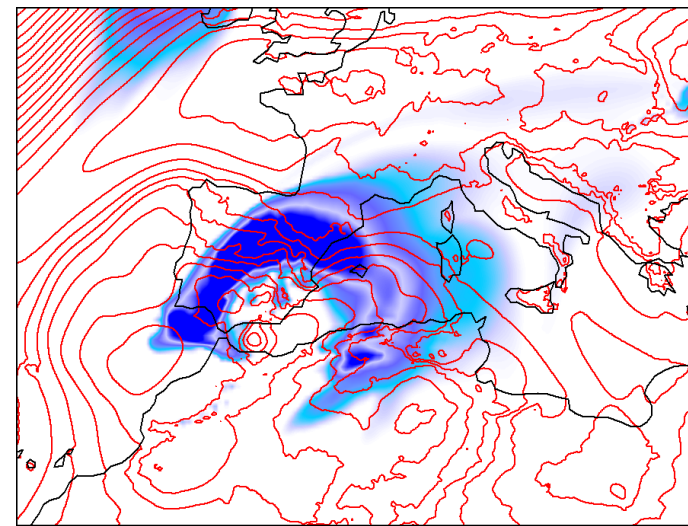
$\Delta M = -0.035 \%$   $\Delta E = +0.200 \%$



Initial



t=36h

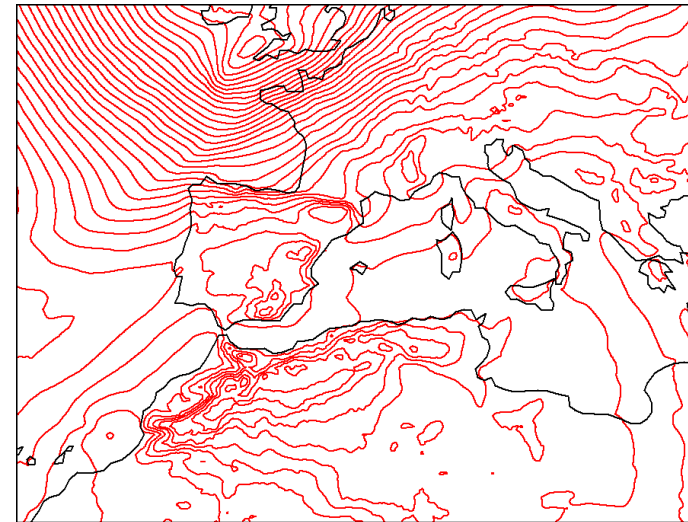
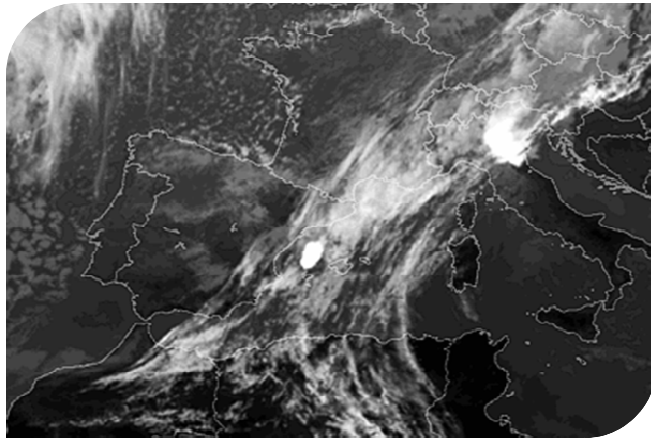




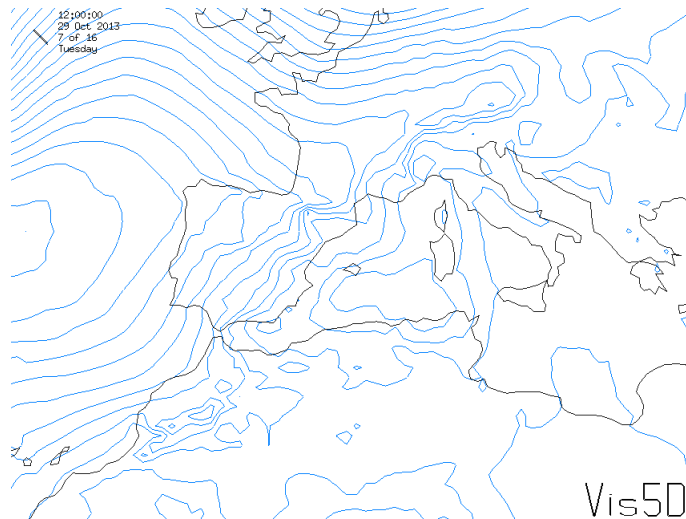
> "MALLORCA" Severe Squall Line (IC: 00 UTC 28 Oct 2013)

(dx=25km, dzm=200m, stretch=10, dt=40s, Nstep=6, 90h)

$\Delta M = +0.511 \%$   $\Delta E = +0.075 \%$



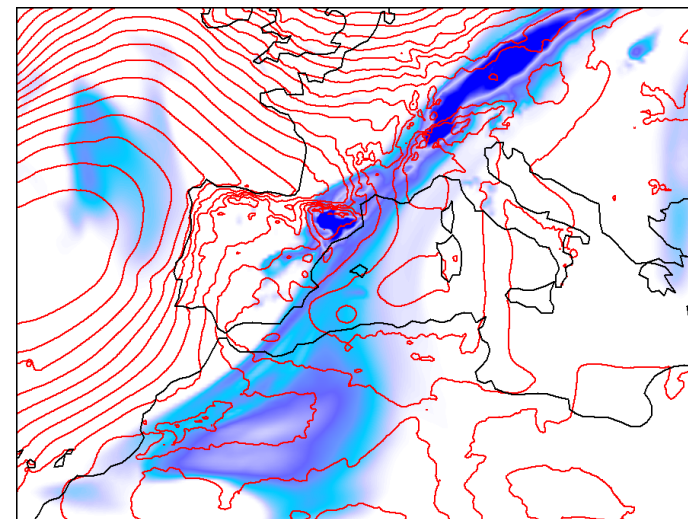
Initial



ECMWF

Vis50

t=36h

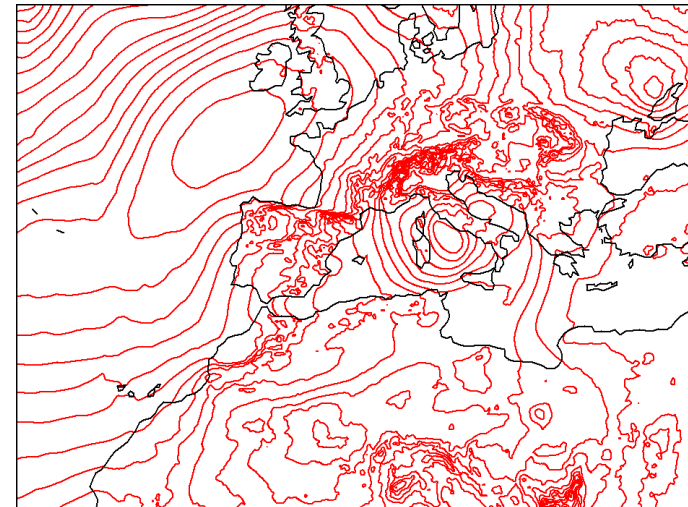


TRAM

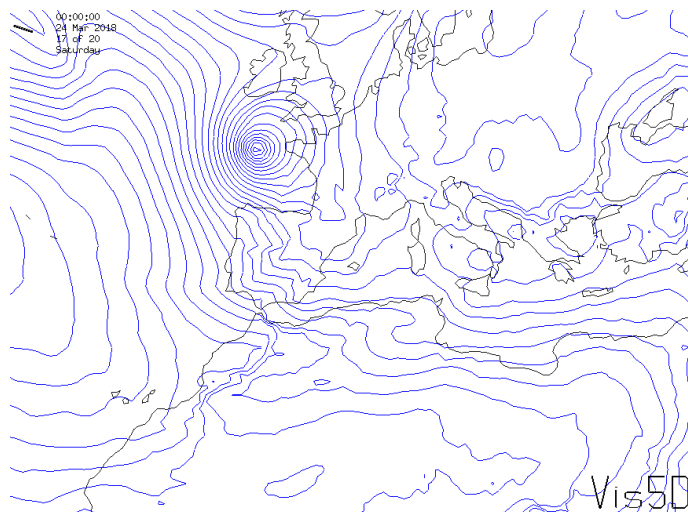
> "BRUNO" Intense Cyclonic Storm (IC: 00 UTC 21 Mar 2018)

(dx=25km, dzm=200m, stretch=10, dt=40s, Nstep=6, 90h)

$\Delta M = -0.533 \%$   $\Delta E = -0.285 \%$



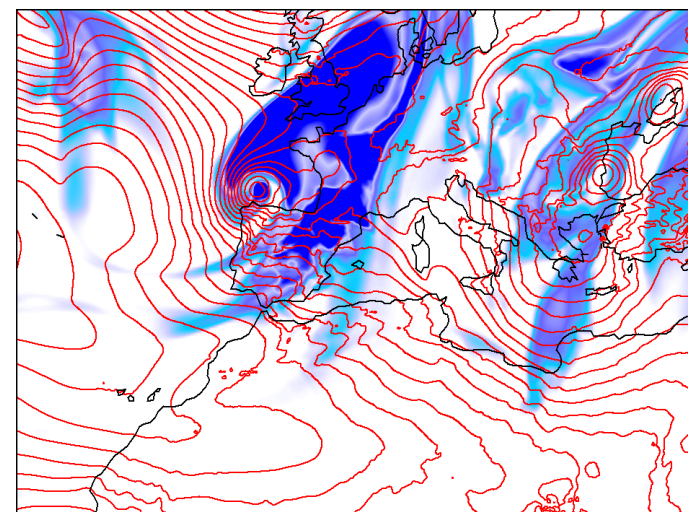
Initial



ECMWF

Vis5D

t=72h



TRAM

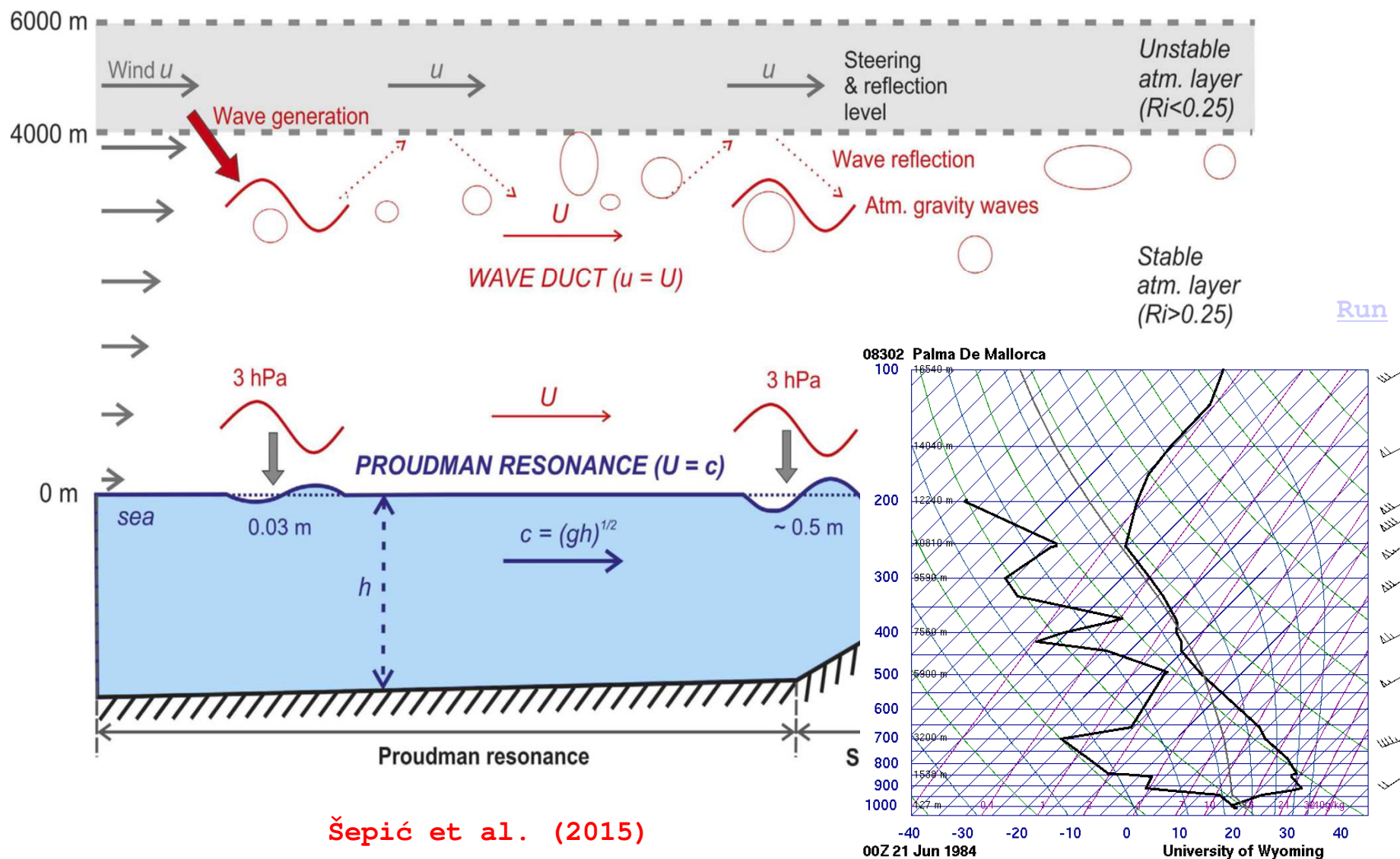
- > **NEW MODEL** achieved (at present just dynamical core) **SUITABLE** to simulate processes ranging from small-scale thermal bubbles ( $\approx 10$  m) to synoptic-scale baroclinic ciclones ( $\approx 1000$  km), including orographic circulations
- > **MAIN CHARACTERISTICS:** Advection form under REA approach (mass & energy not strictly conserved); Fully compressible & Non hydrostatic; Time-splitting strategy; Vertically semi-implicit; Triangle-based horizontal mesh (no staggering); Z-coordinate (no staggeging) allowing arbitrary stretching (proper treatment of slopes and bottom BCs); Lambert projection with all Coriolis and curvature terms retained; No explicit filters needed
- > A variety of comparison tests showed that **TRAM PERFORMS AT LEAST AS WELL** as state-of-the-art models

- > **COMPLETE TRAM** with appropriate **PHYSICS** package (fast approach: **WRF-based** parameterization schemes); Reexamine the real cases and consider new tests (e.g. simulation of convective & precipitation systems)
- > **OPTIMIZE THE PERFORMANCE** (i.e. reduce running times) of TRAM in our computer platforms, beyond the current adaptation to shared-memory systems using the OpenMP directives
- > **EXPLOIT THE CAPABILITIES** of the new tool in the academic and research arena, with particular focus on regional problems (e.g. "**Rissaga Study**")



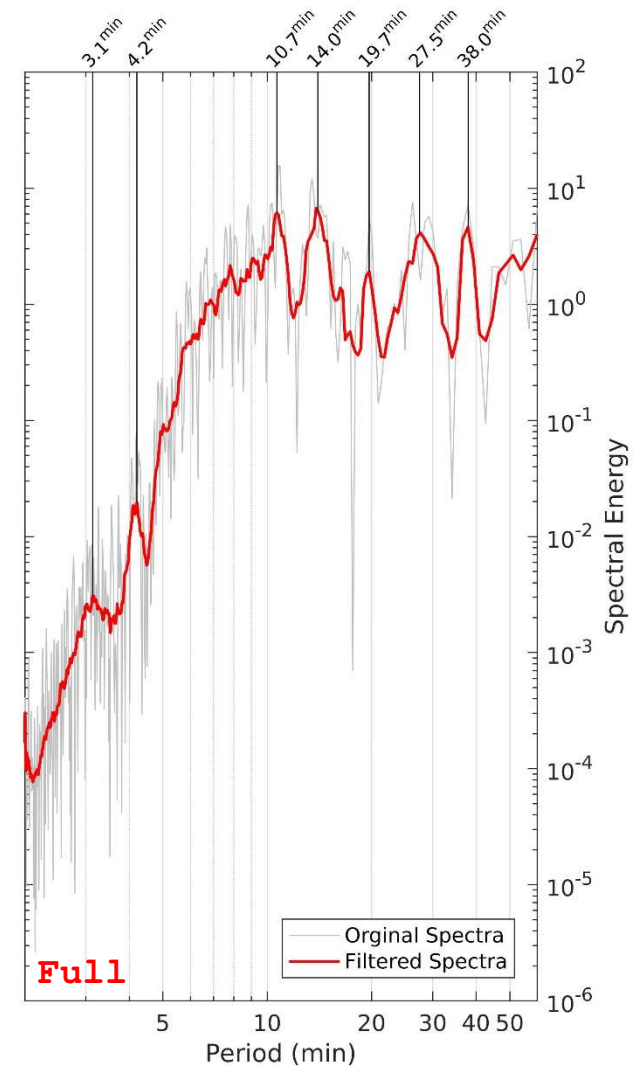
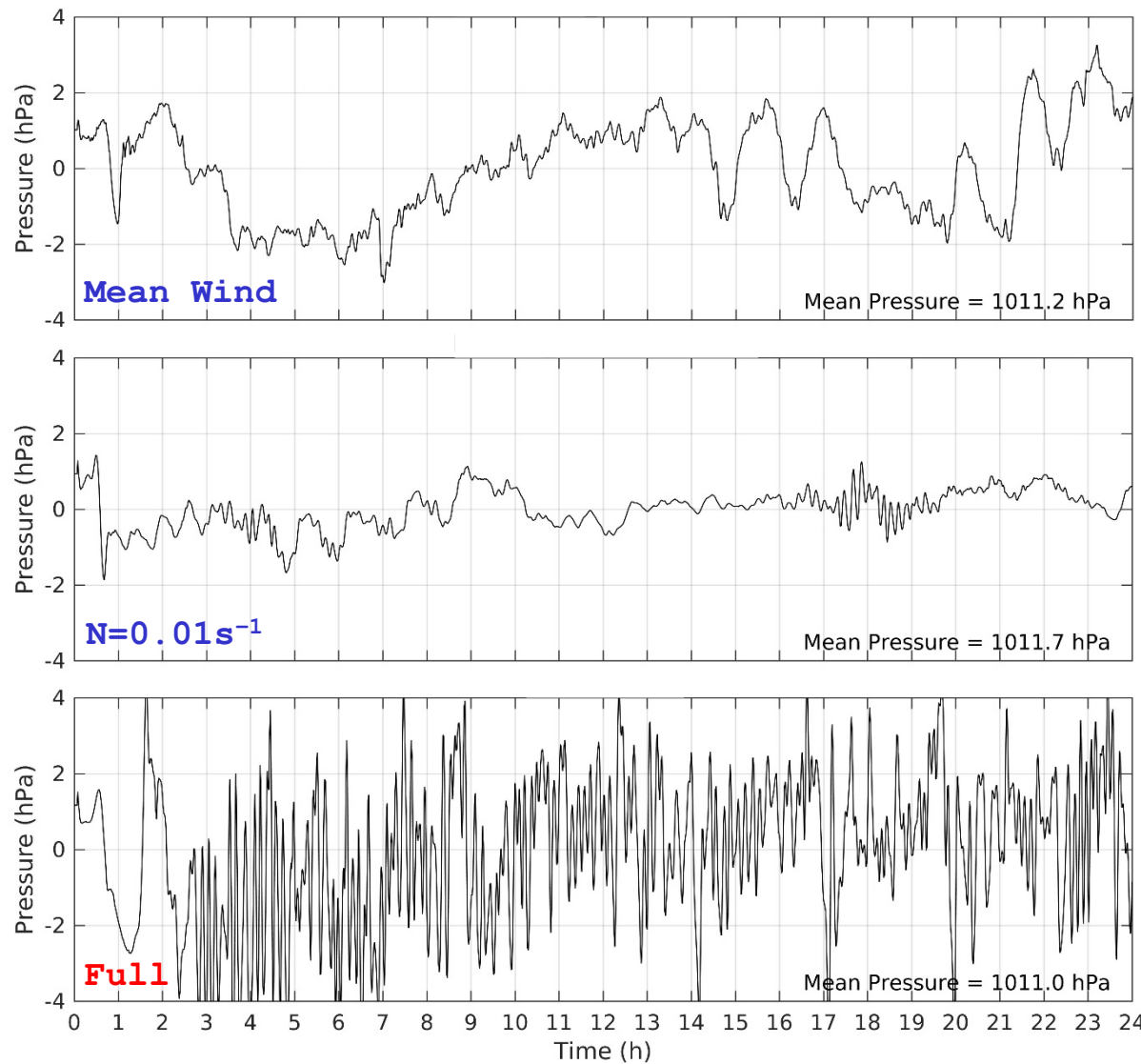
## > "Rissaga" Study

( $dx=250m$ ,  $dzm=250m$ ,  $stretch=5$ ,  $dt=0.75s$ ,  $Nstep=10$ , **24h**)



## > "Rissaga" Study

(dx=250m, dzm=250m, stretch=5, dt=0.75s, Nstep=10, 24h)





**THANK YOU**  
*for*  
*your attention*